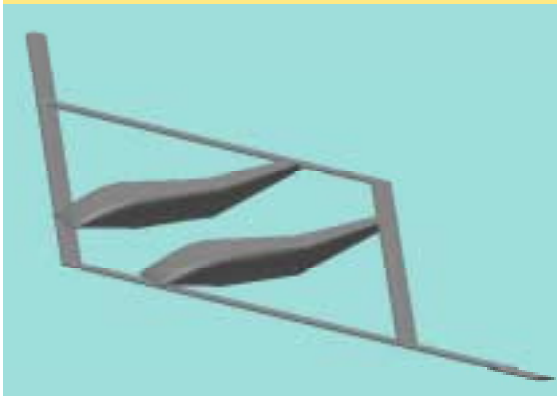


Nov 2002, Presentation UAV Workshop, Bath University

TOWARDS DESIGNING HIGH ASPECT RATIO HIGH ALTITUDE JOINED-WING SENSOR- CRAFT (HALE-UAV)



Dr. R. K. Nangia

Bsc PhD CEng AFAIAA FRAeS

**Nangia Aero Research Associates,
BRISTOL, UK.**

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- Lastly, any opinions expressed are those of the author.

This Presentation

- Introduce HALE-UAV
- A Vision of Future – Sensor Craft Importance
- Joined-Wing Configs.
- 2-D Laminar Aerofoils
- Aspects of 3-D Design, different Swept Tips
- LE Suction Control, Elliptic loadings, Neutral Stab.
- CFD Checks
- Inverse 3-D Design Capabilities
- Intake Design – Preliminary Work
- Avenues for Further Work

Typical HALE Global Hawk

span: 116 ft, length 44 ft

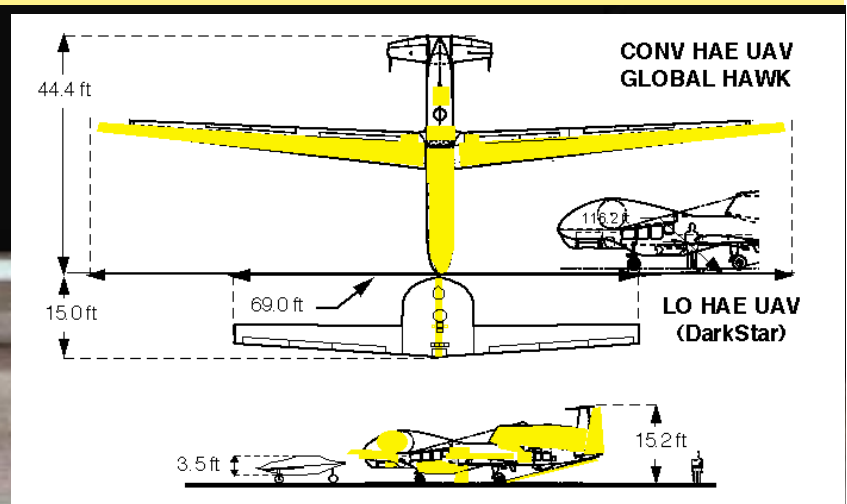
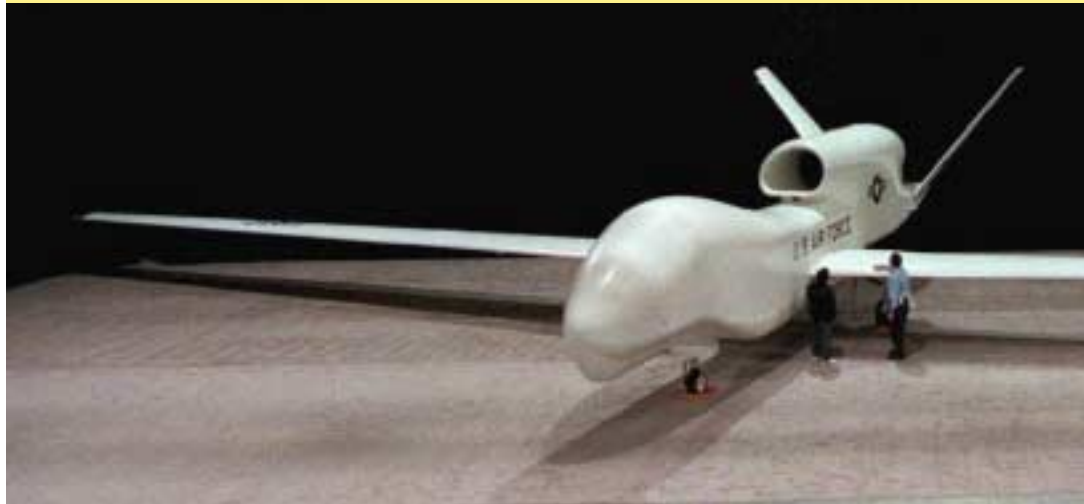
light composites, aluminium fuselage, COST \$10M

Range 12000 nm, AUW 25,600 lb , range up to 2000nm at 65000ft

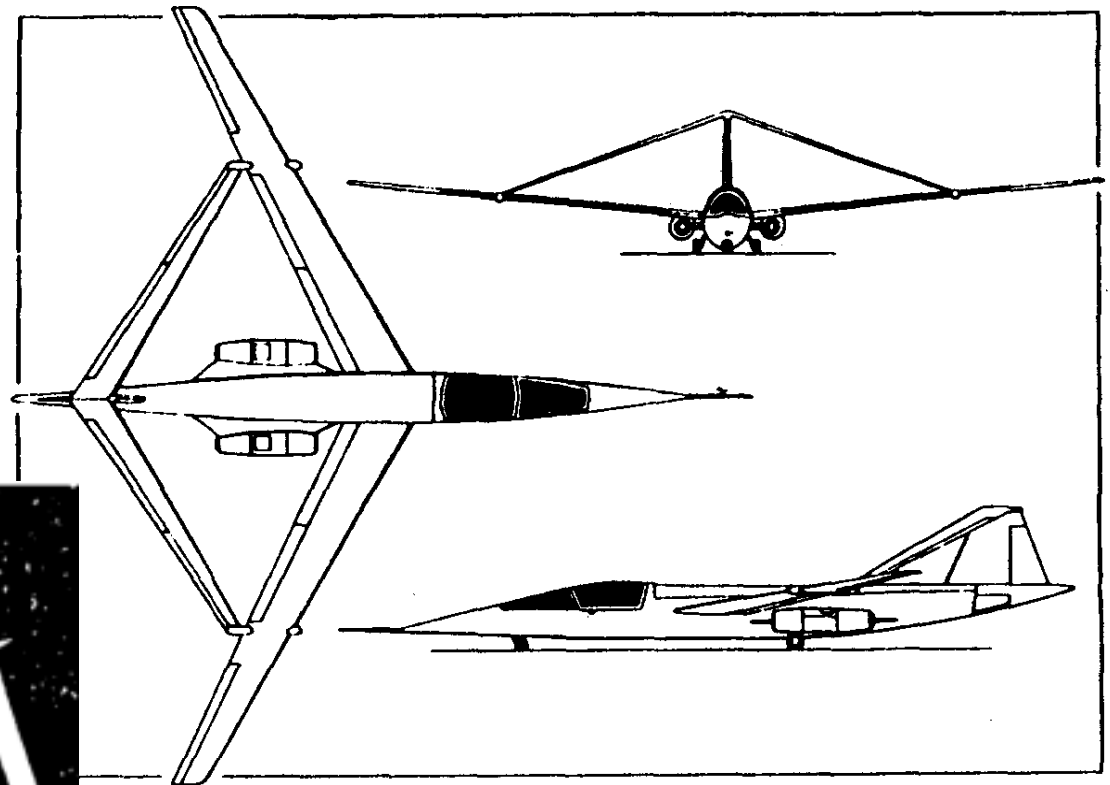
flies to an area 1200 miles and remains on station 24 hrs

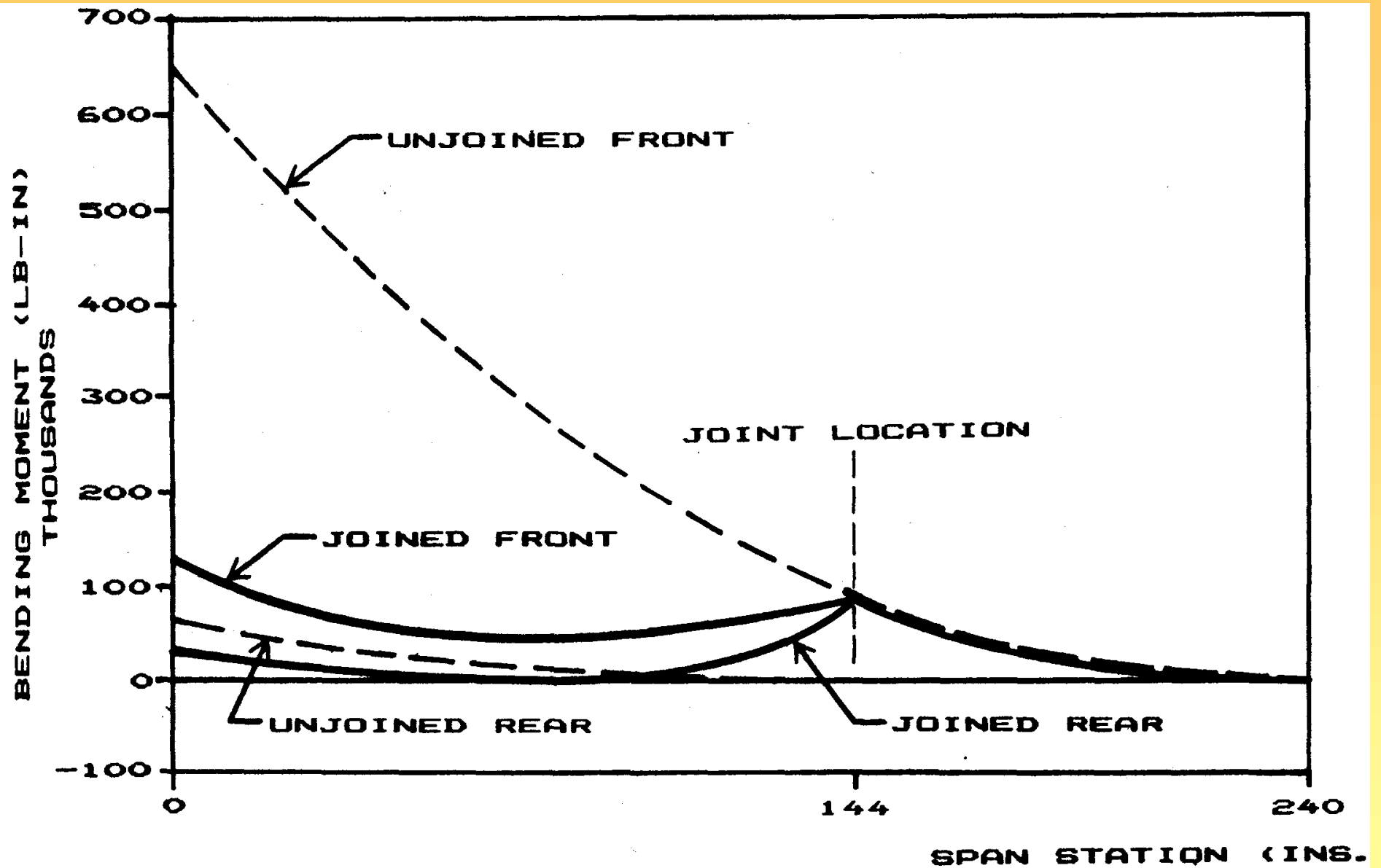
cloud penetrating synthetic aperture radar /
ground moving target indicator, electro-optical and infra-red sensors

image an area 40,000 square miles (State of Illinois) in 24 hours



WOLKOVITCH

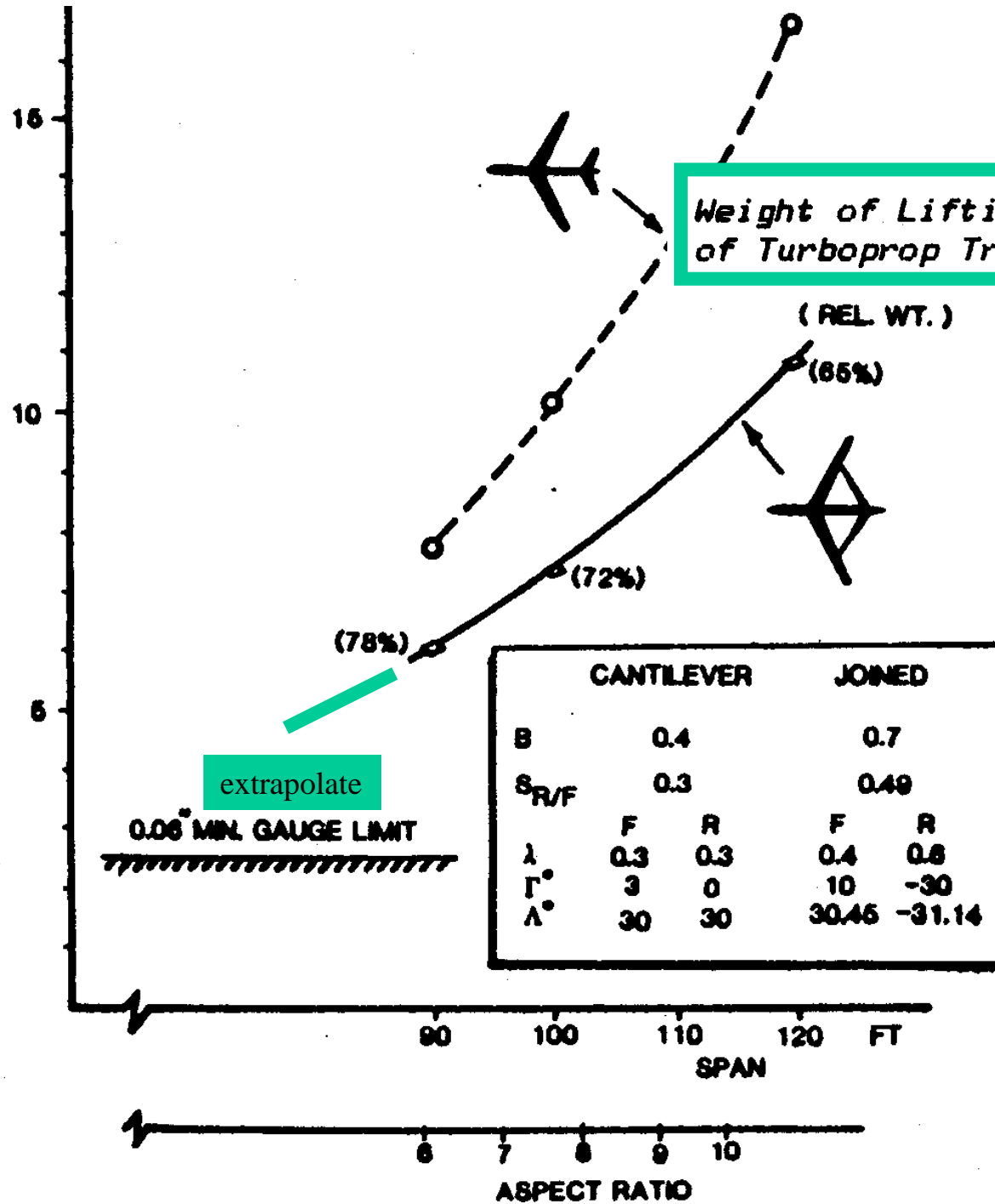


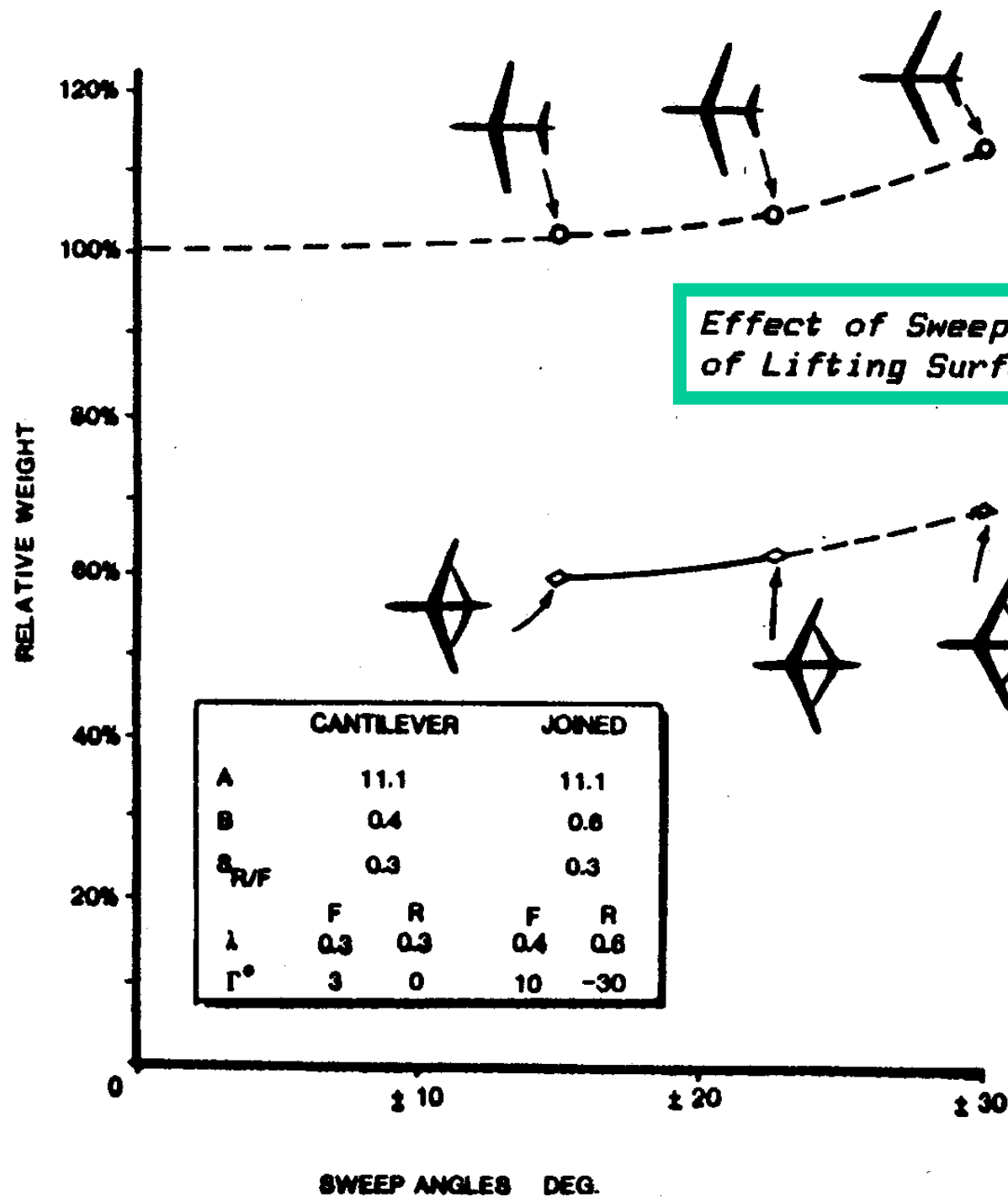


Bending Moments acting on an Inboard-Jointed Jointed Wing.

WEIGHT OF LIFTING SURFACES x 1,000 lbs.

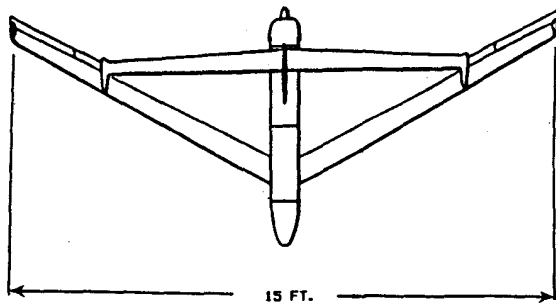
Weight of Lifting Surfaces
of Turboprop Transports Versus Aspect Rat





*Effect of Sweep on Relative Weight
of Lifting Surfaces of Turboprop Transport*

Guess !



11. ACA Industries "LAURA" Long Endurance Remote Vehicle.

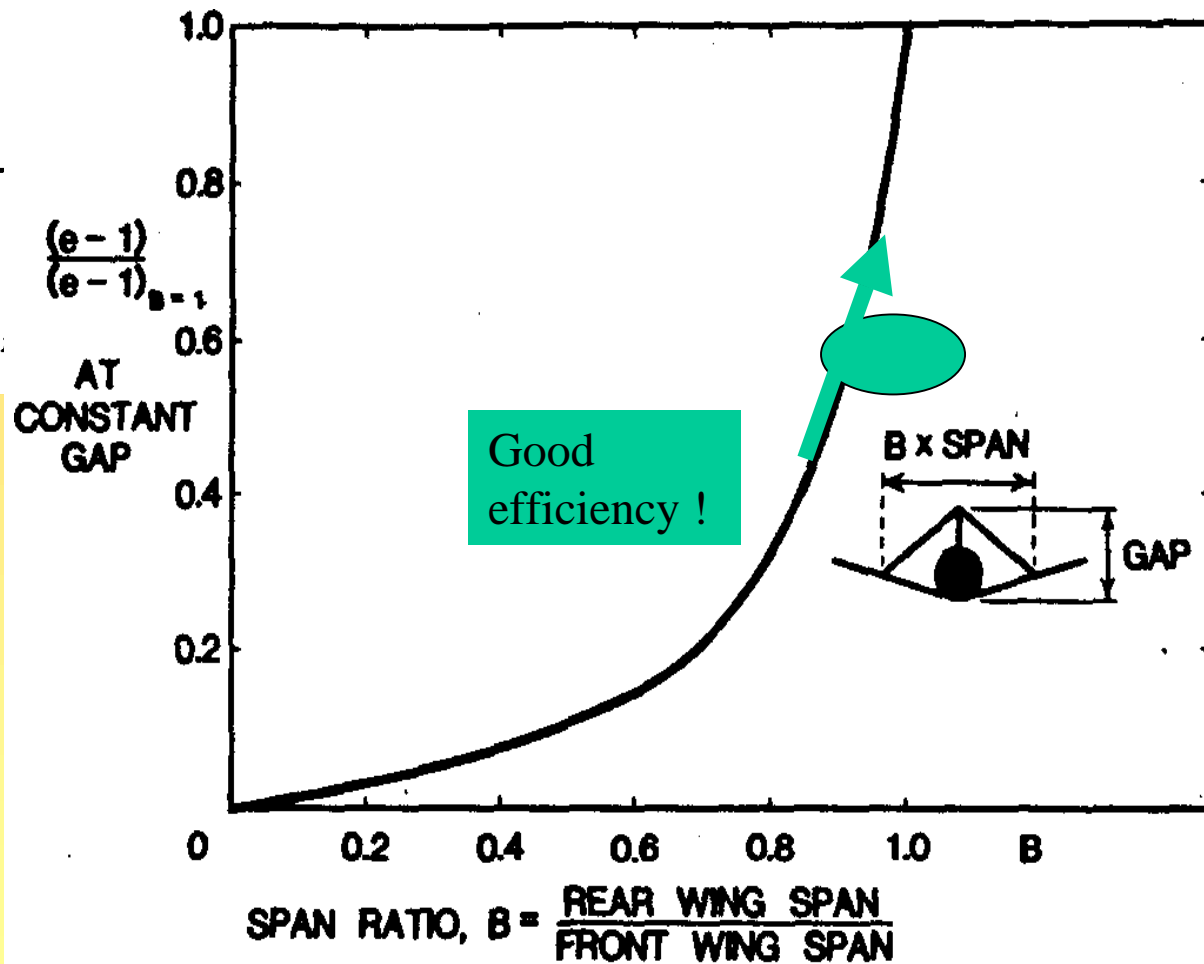
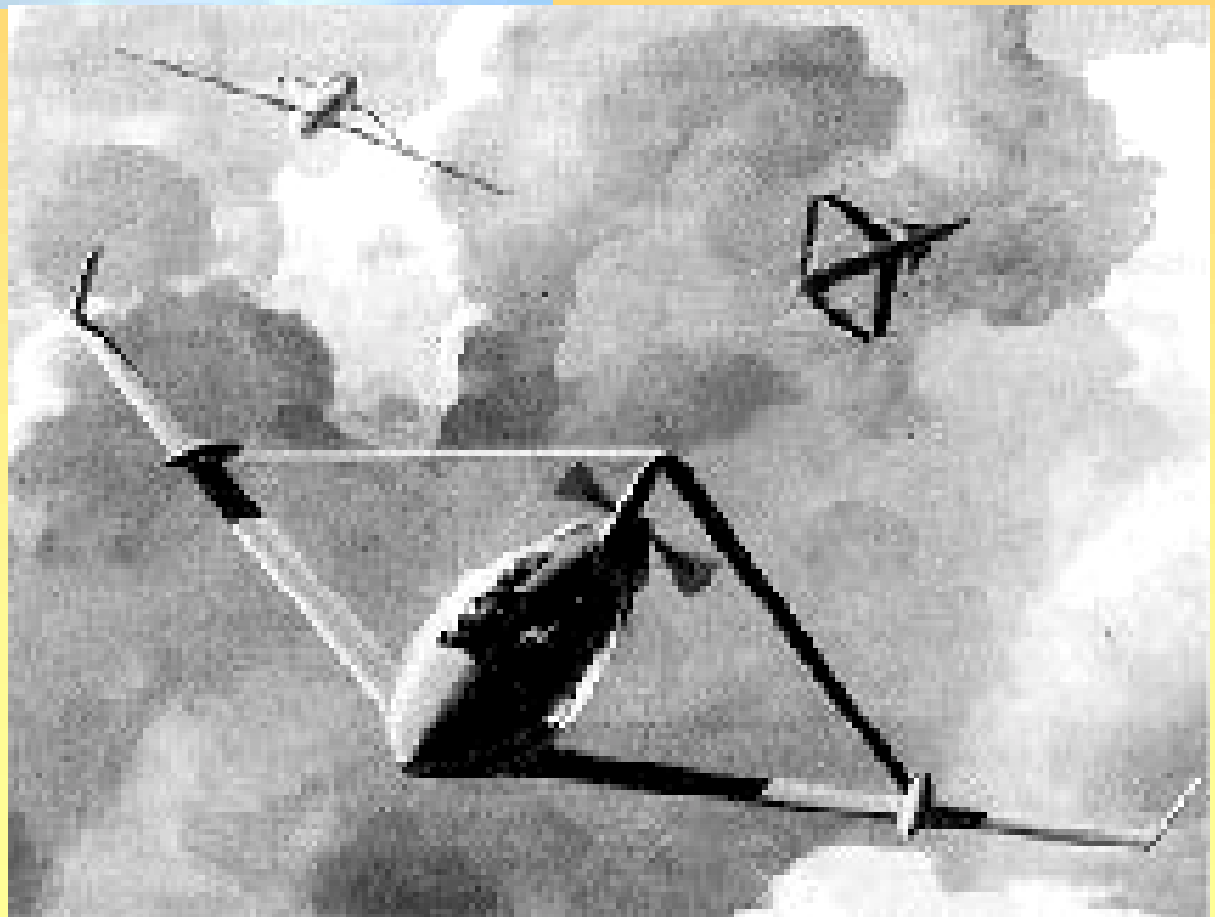
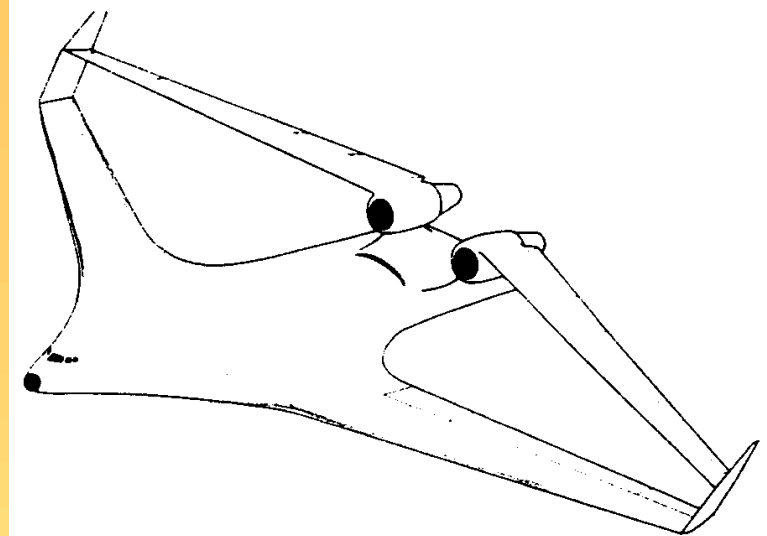


Fig. 12. Effect of Span Ratio on Span-Efficiency Factor.

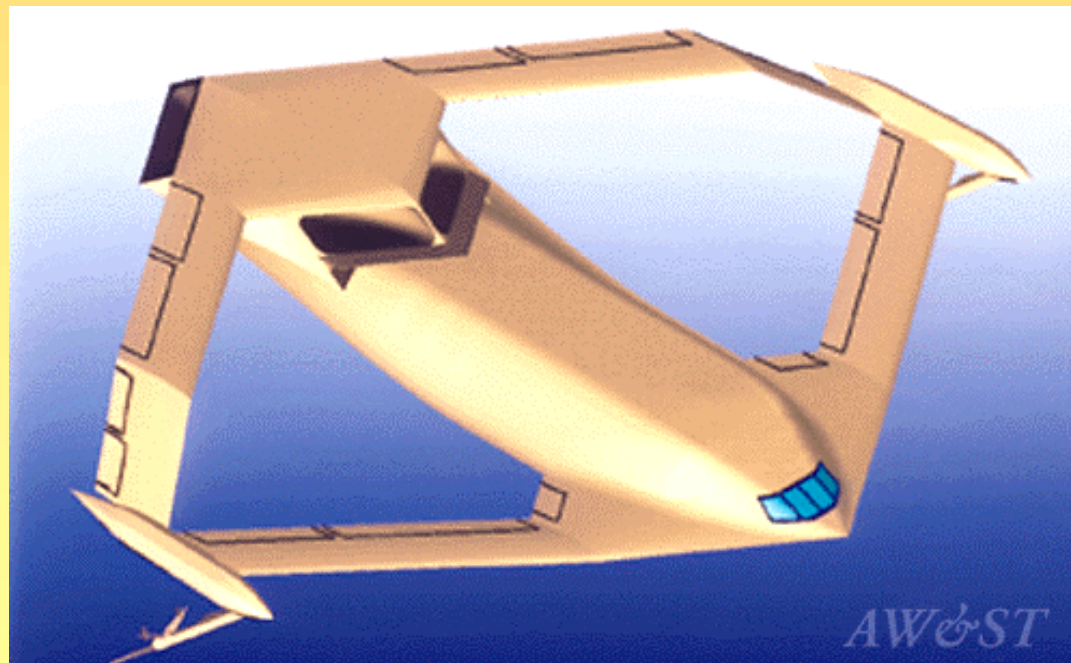




TANKERS



TRANSPORTS

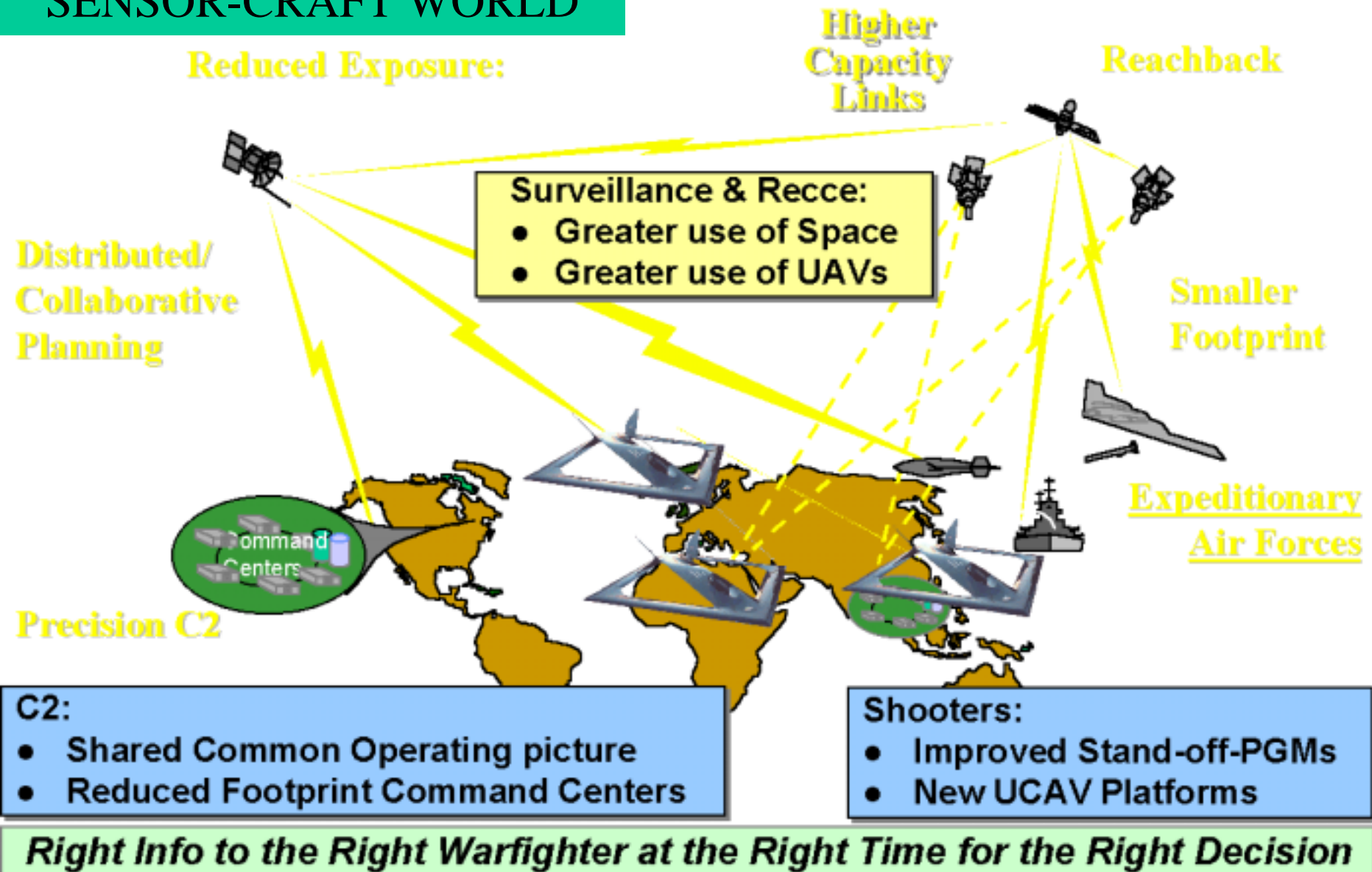


Joined-Wing Transport Concept Features A Refueling Boom On Each Wingtip And More Control Surfaces Than Conventional Aircraft



AC2ISR: What the Future Will Bring

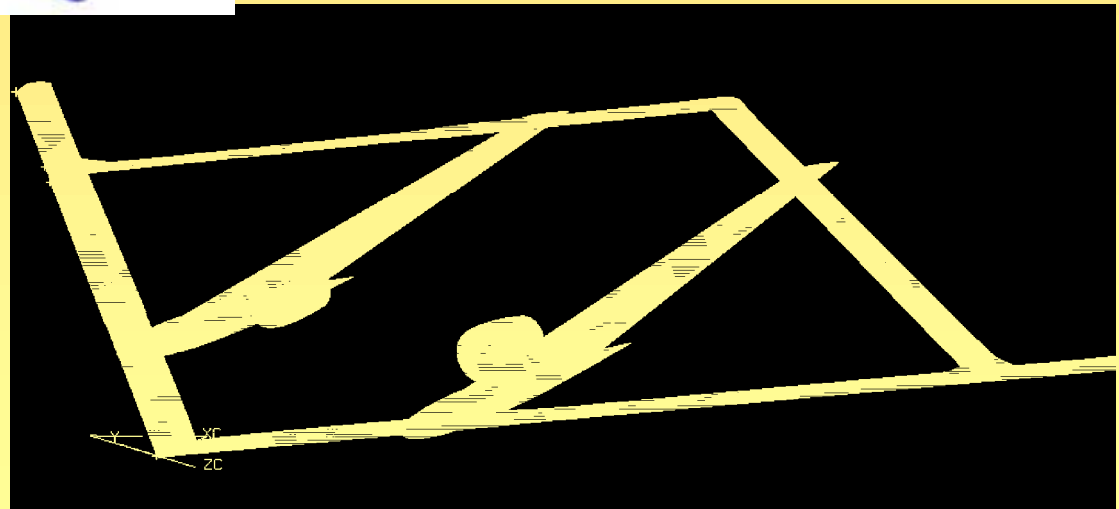
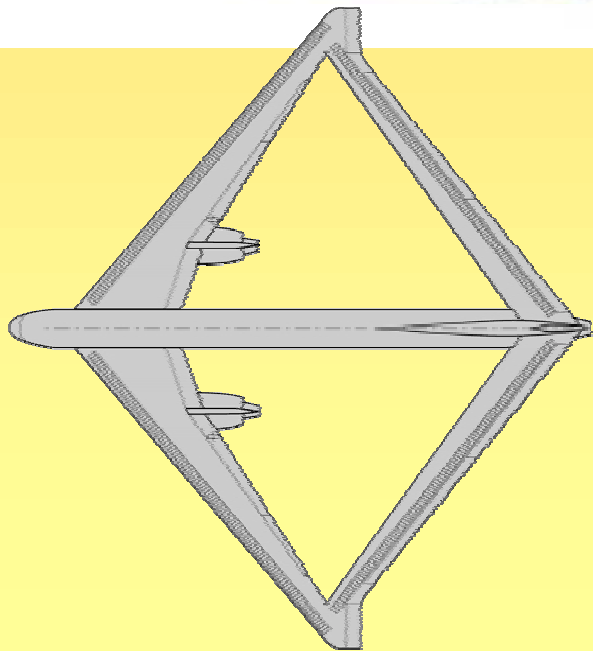
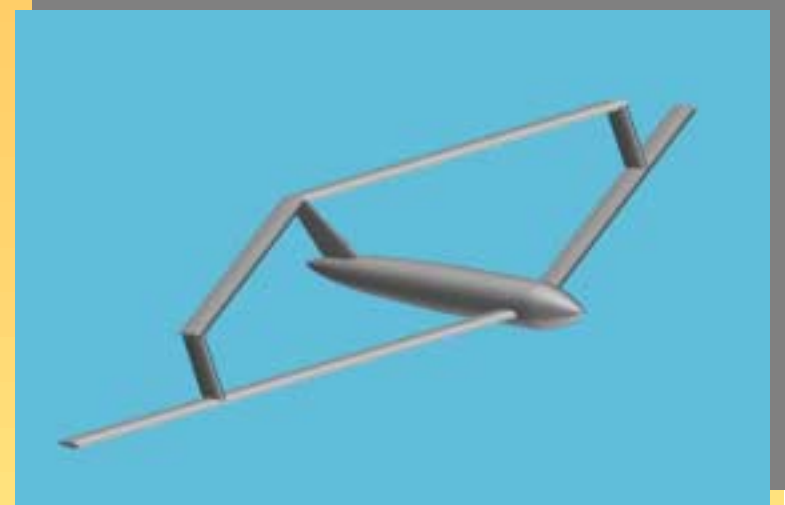
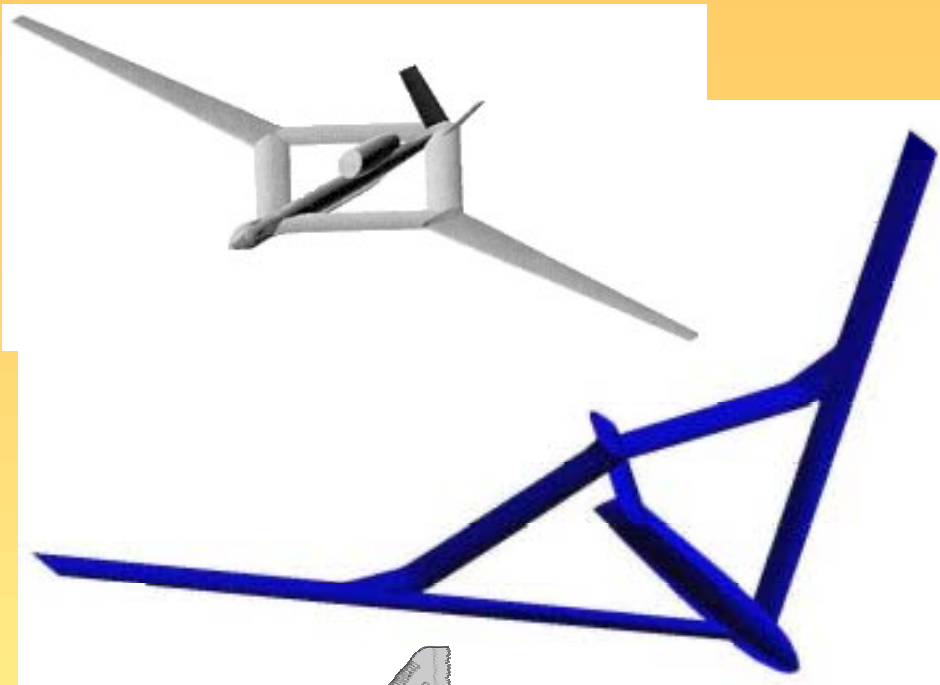
SENSOR-CRAFT WORLD



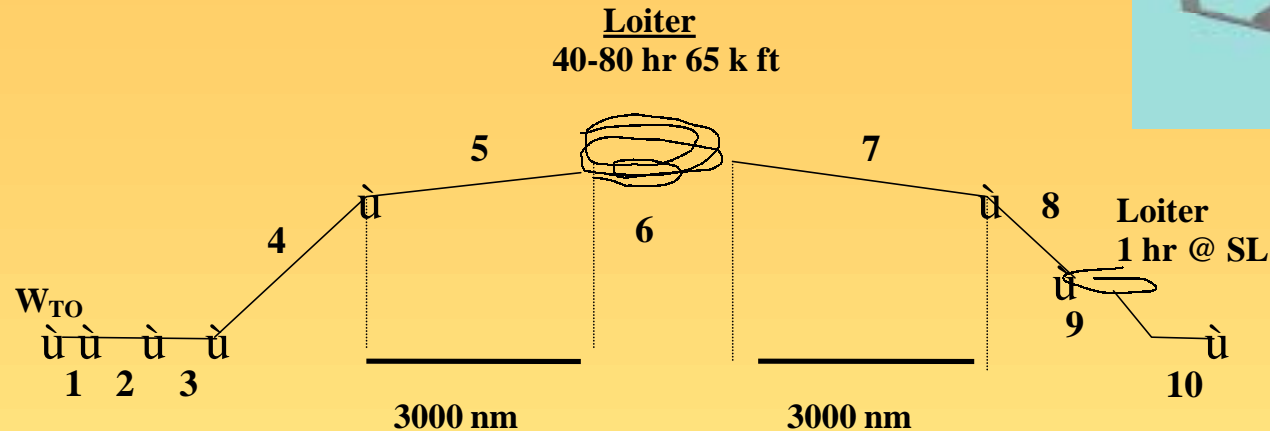
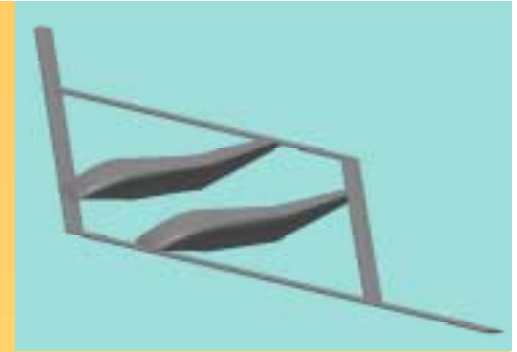
Sensor Craft UAV as Element of Global Awareness/Global Engagement Vision



Other joined-wing possibilities



Mission profile and requirements



Mission Segments

1. Engine Start & Warm-up
2. Taxi
3. Takeoff
4. Climb & Accelerate to Cruise
5. Cruise out 3000
6. Loiter
7. Return Cruise
8. Descend
9. Loiter at Sea Level
10. Landing, Taxi, Shutdown

Cruise Radius: 3000 nm

Loiter: 65 Kft for 40 - 80 hr (at 3000 nm range)

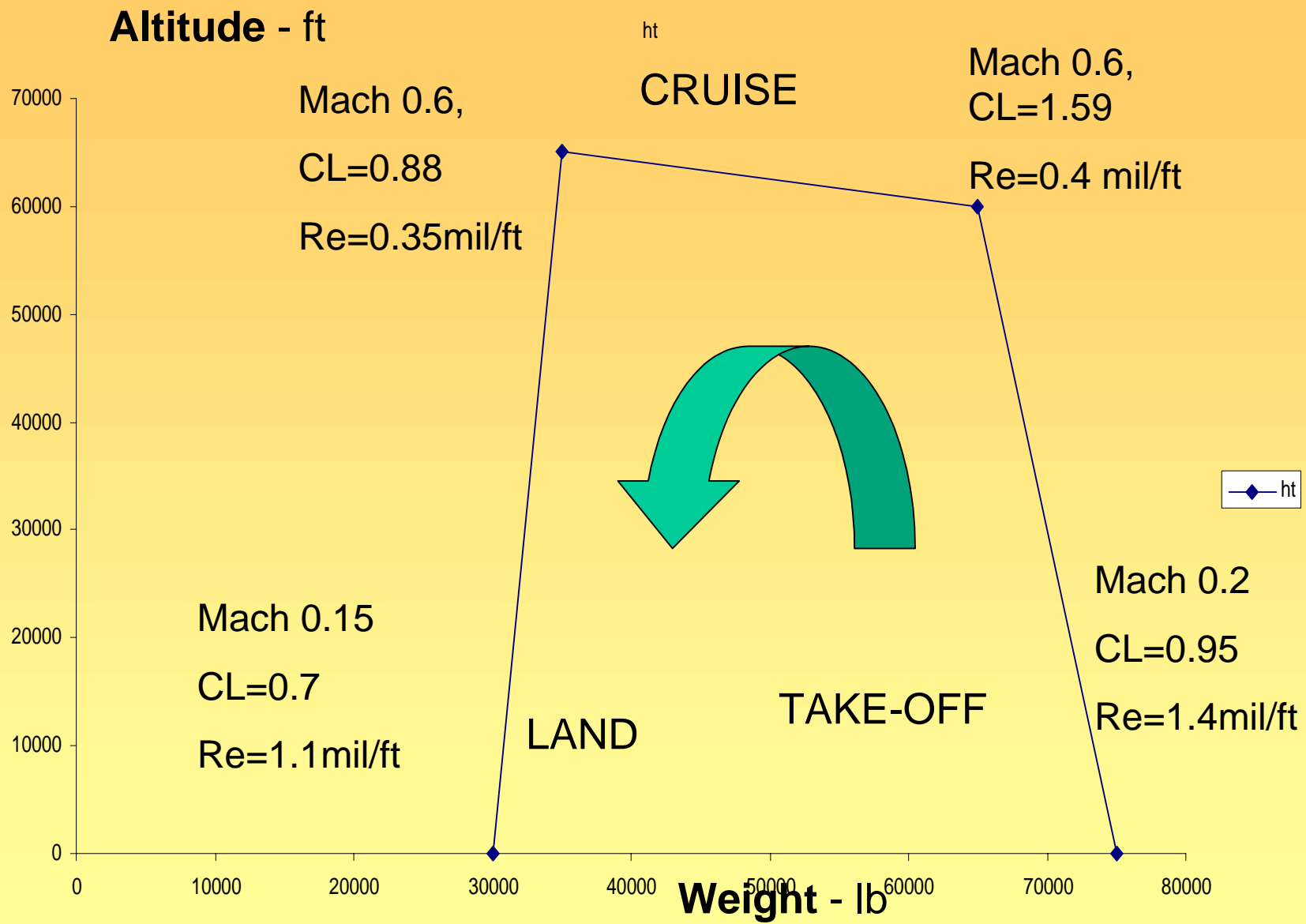
Payload: 4000 lb Field Length: 5350 ft over 50 ft Obstacle (SLS)

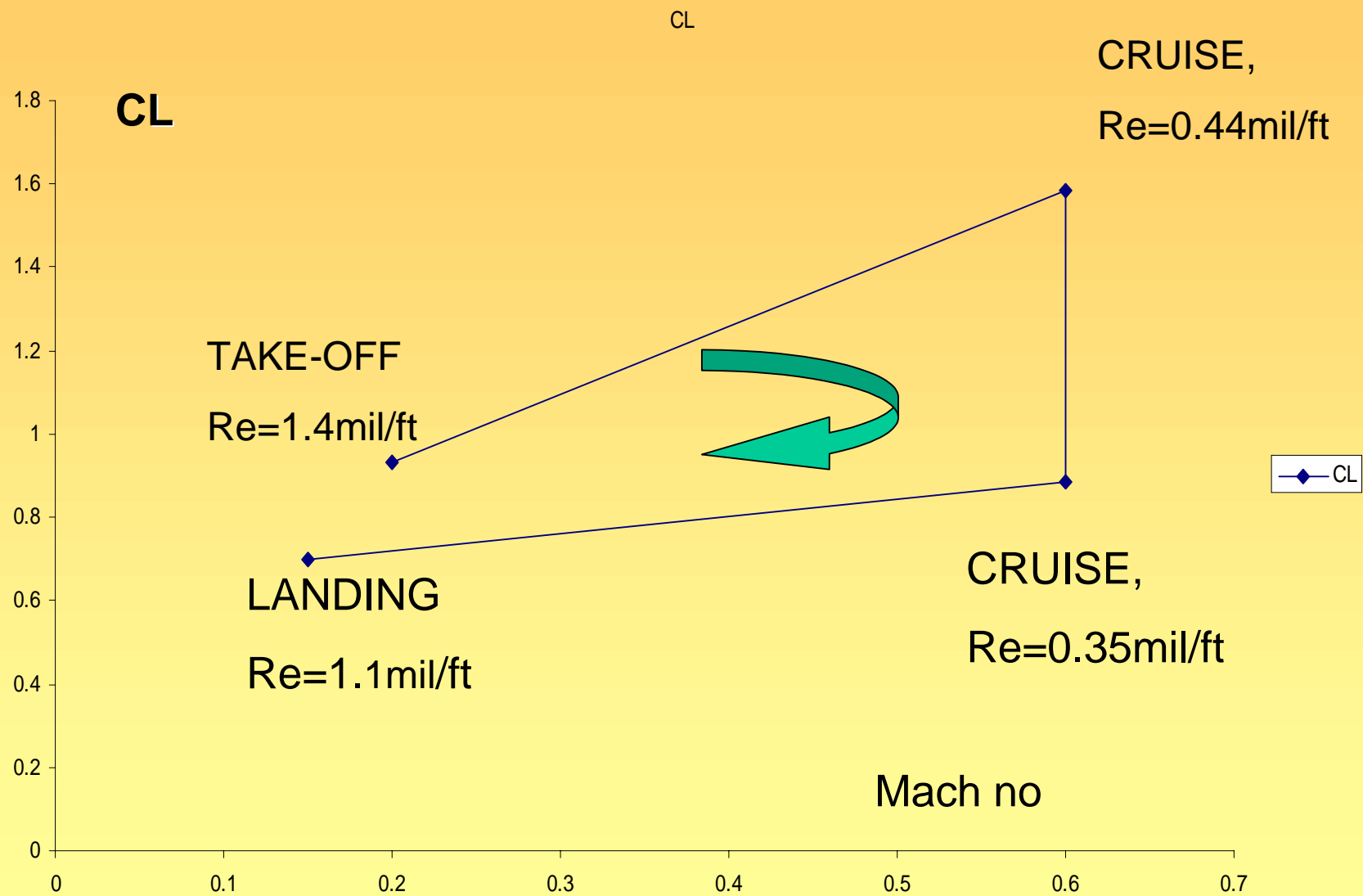
Control: 20 kt cross-wind on takeoff and landing

Flight duration 4-6 days
Implies a Wide Flight Envelope

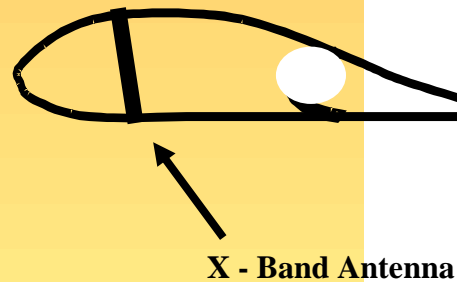
W/S range of interest: 30 - 60

T/W range of interest: .30 -.50

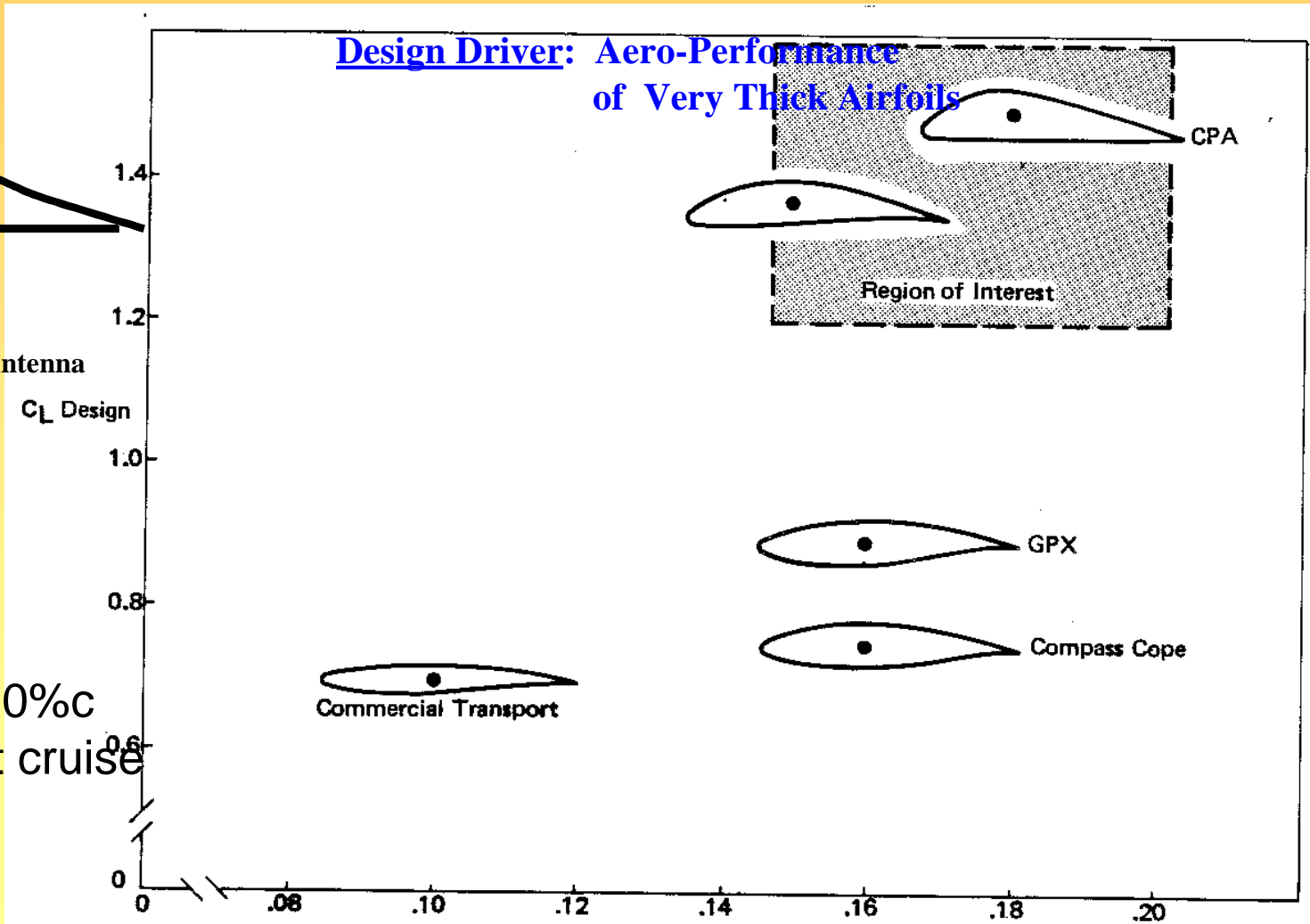


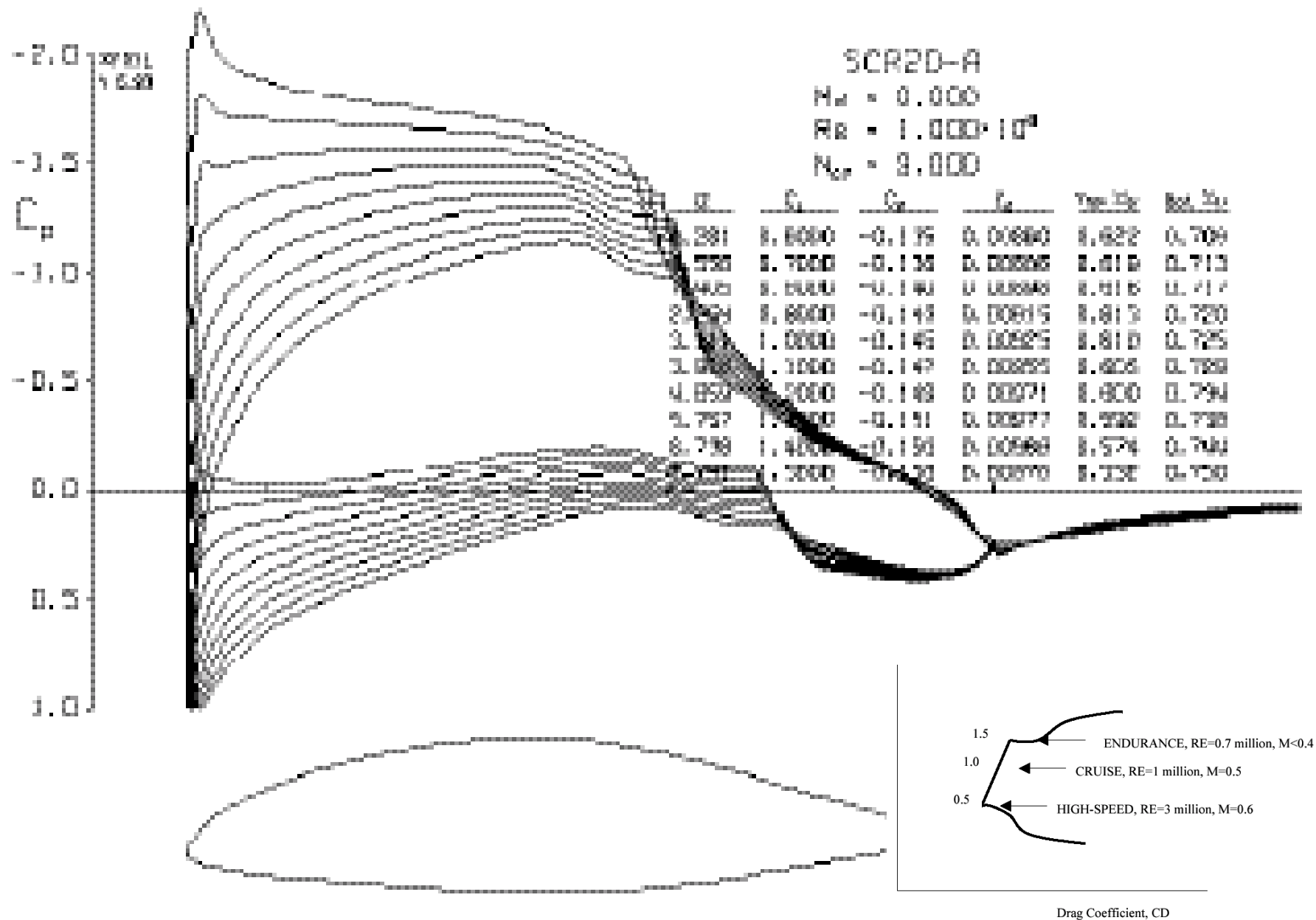


Reference Configuration - Antenna Integration



2-D Driver
High t/c
High L/D
Laminar Flow 50%c
Critical Mach at cruise
Low Re

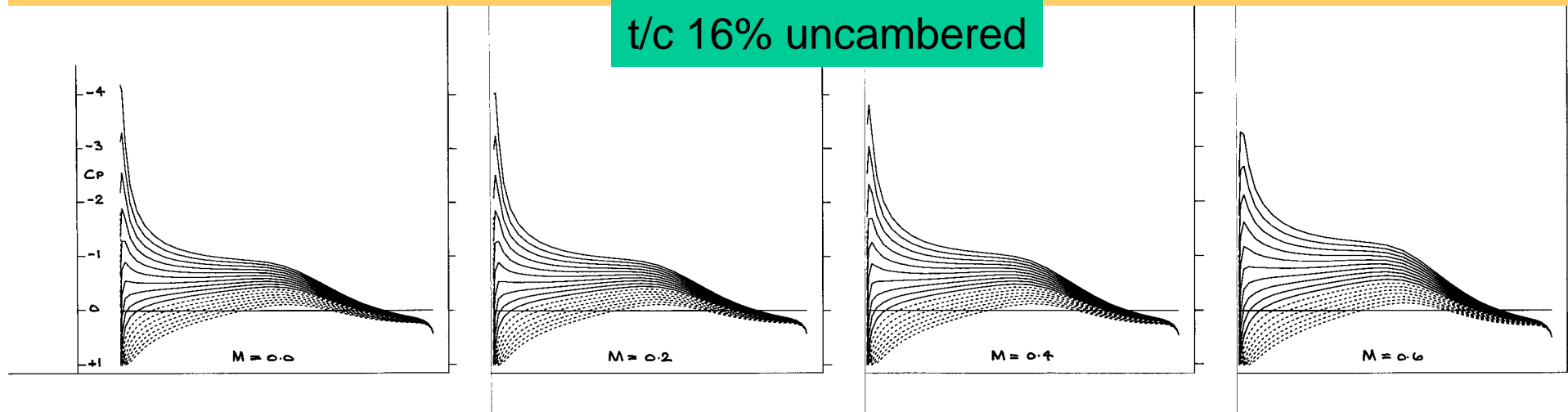




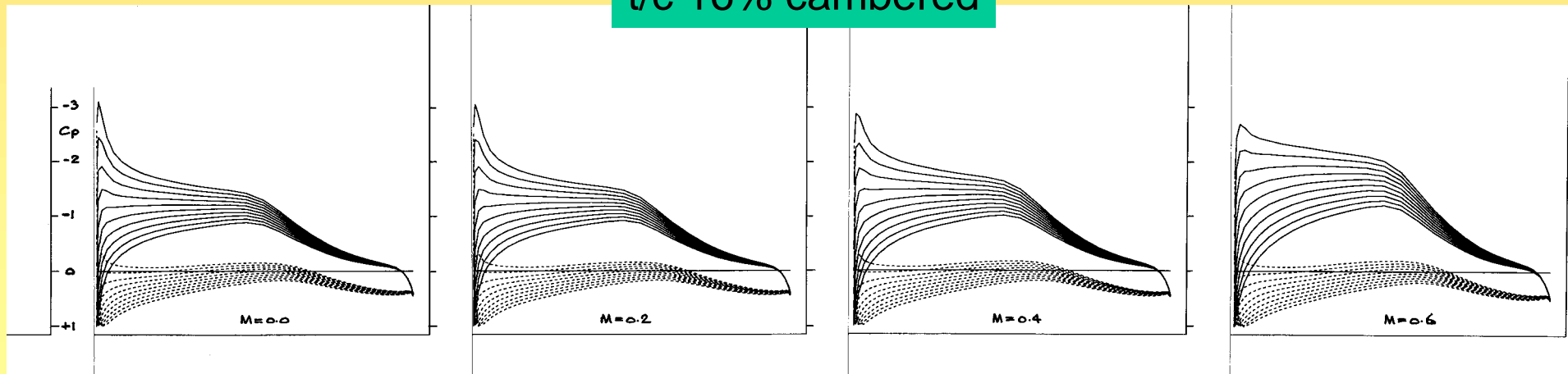
19.6% t/c, Navier-Stokes Results at Re 1 million, Mach 0.01, Biber & Tilmann

2-D CALCULATIONS, INVISCID, MACH no VARIES from 0.0 to 0.6

t/c 16% uncambered

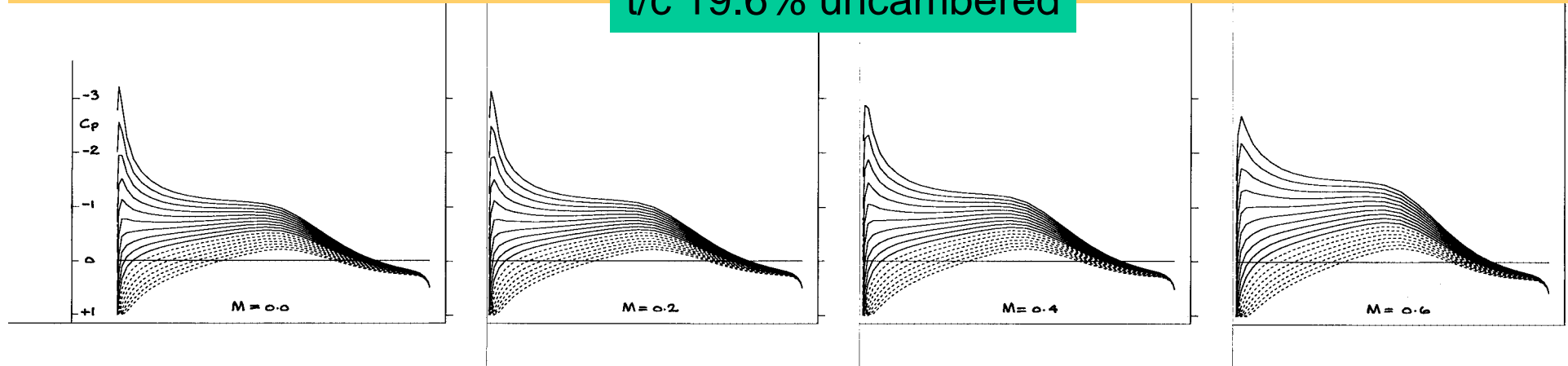


t/c 16% cambered

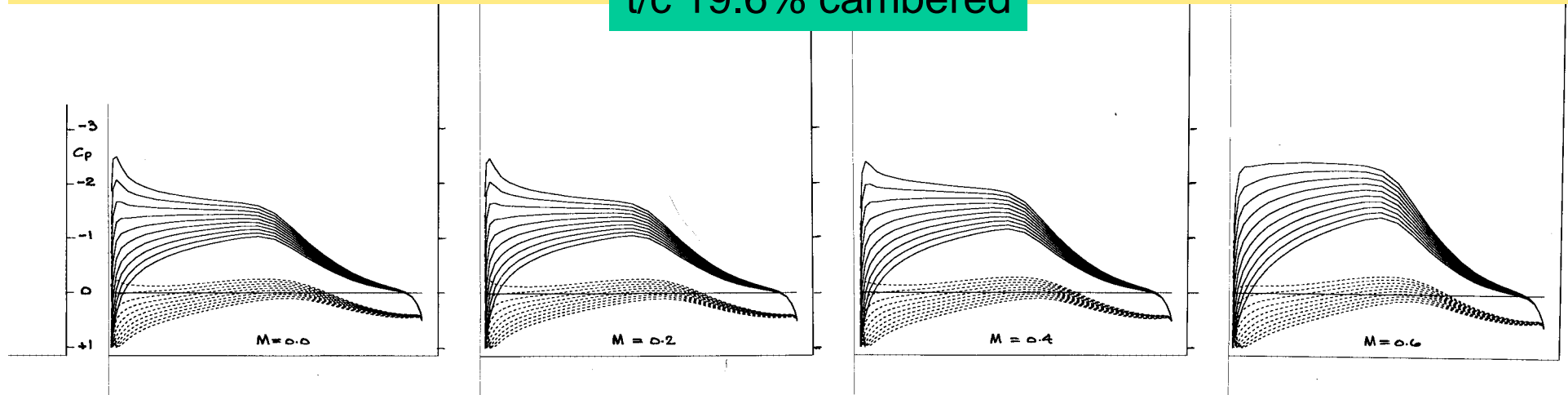


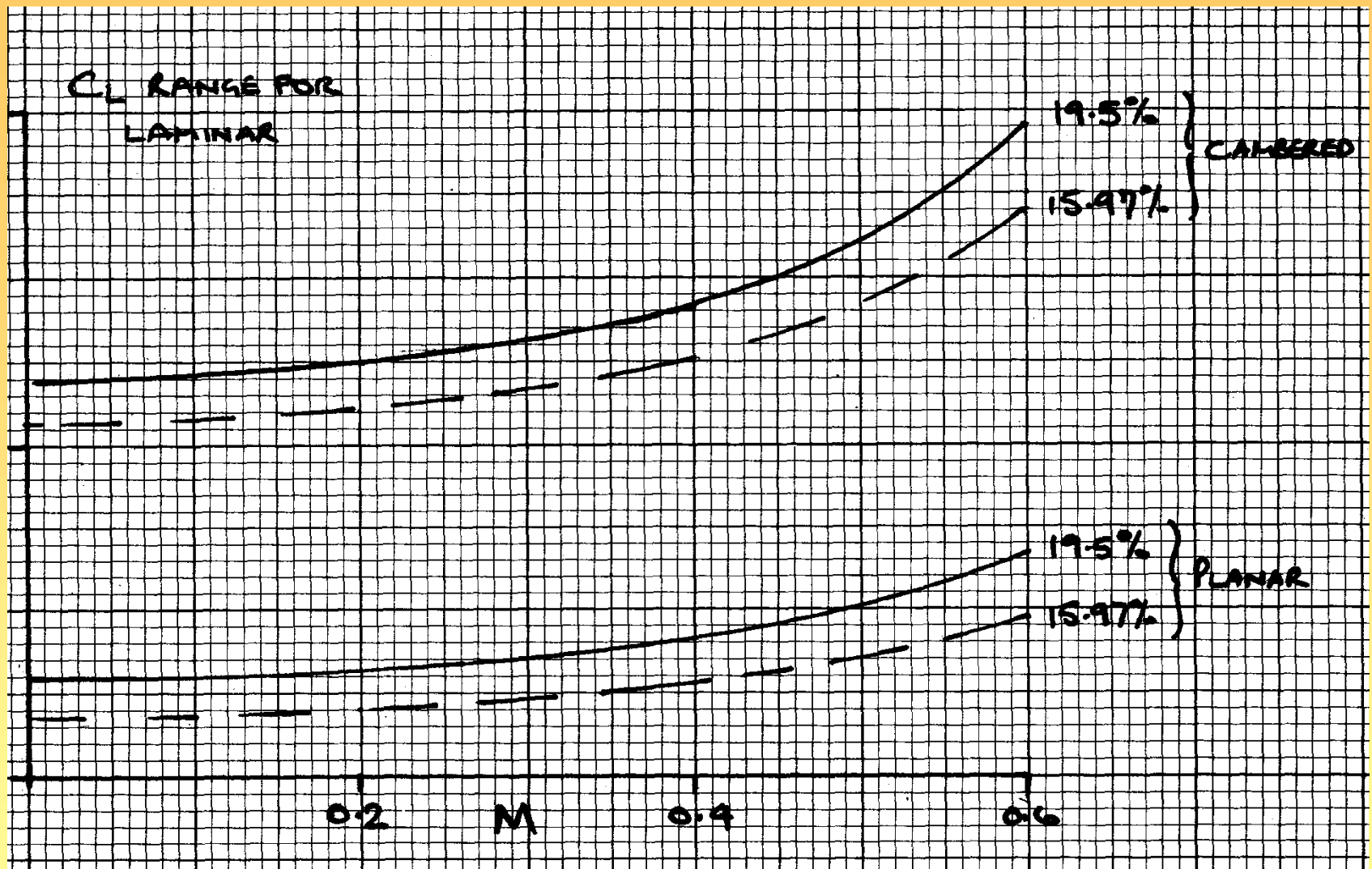
2-D CALCULATIONS, INVISCID, MACH no VARIES from 0.0 to 0.6

t/c 19.6% uncambered



t/c 19.6% cambered





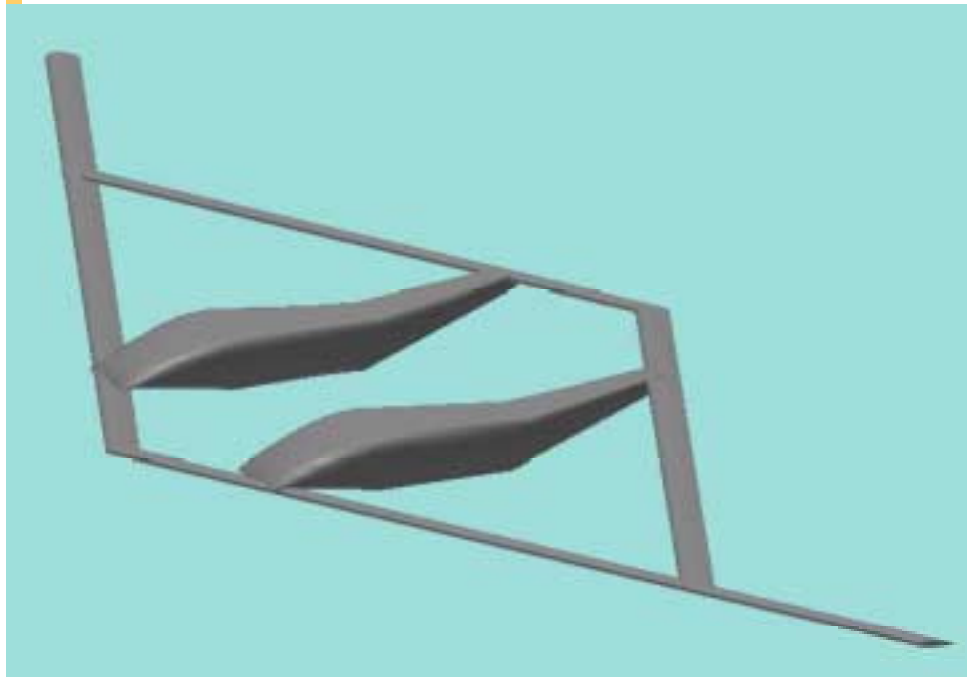
SUMMARISING THE AEROFOIL PERFORMANCE,
LAMINAR FLOW CAPABILITY Uncambered & Cambered

Reference Configuration

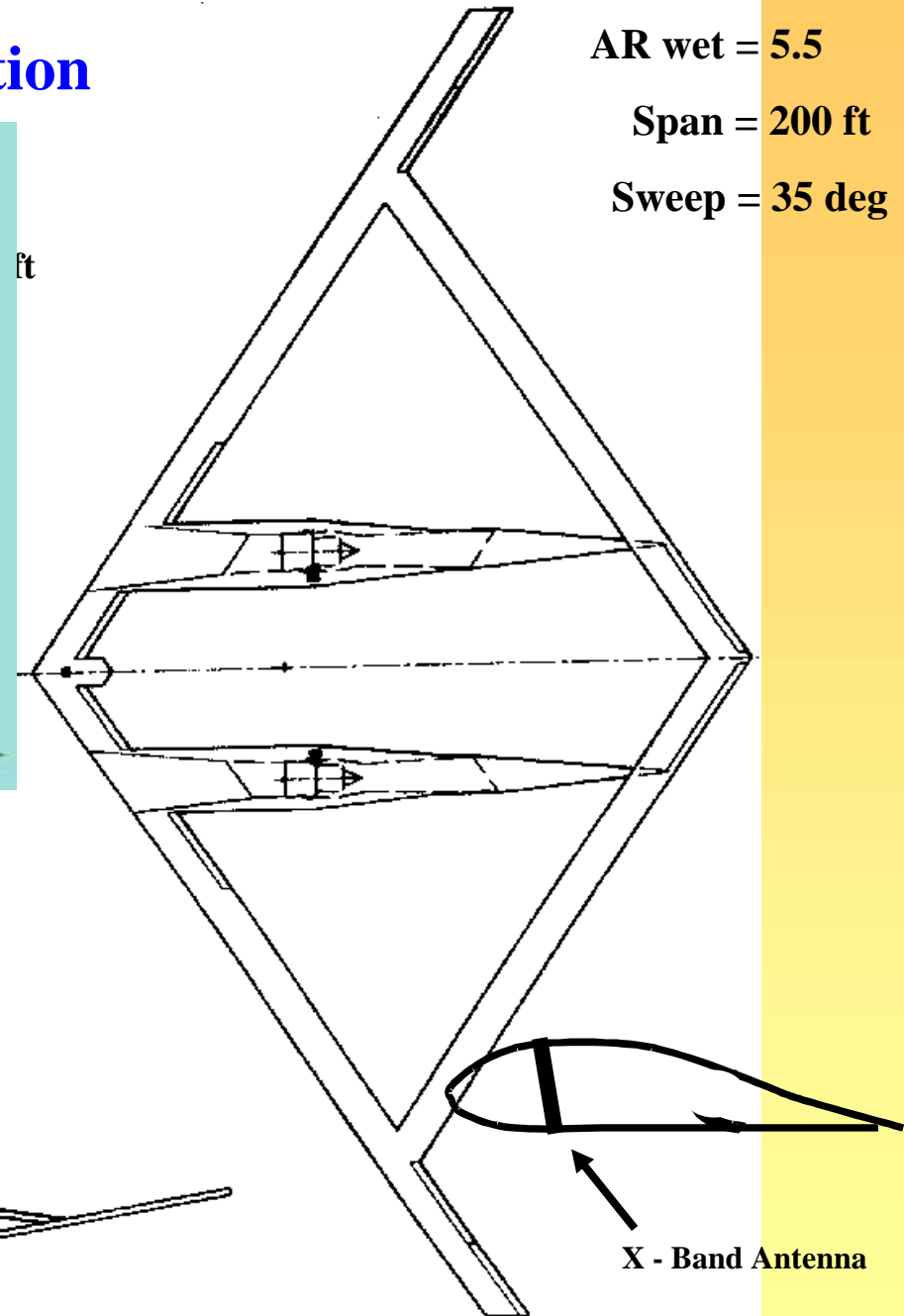
AR wet = 5.5

Span = 200 ft

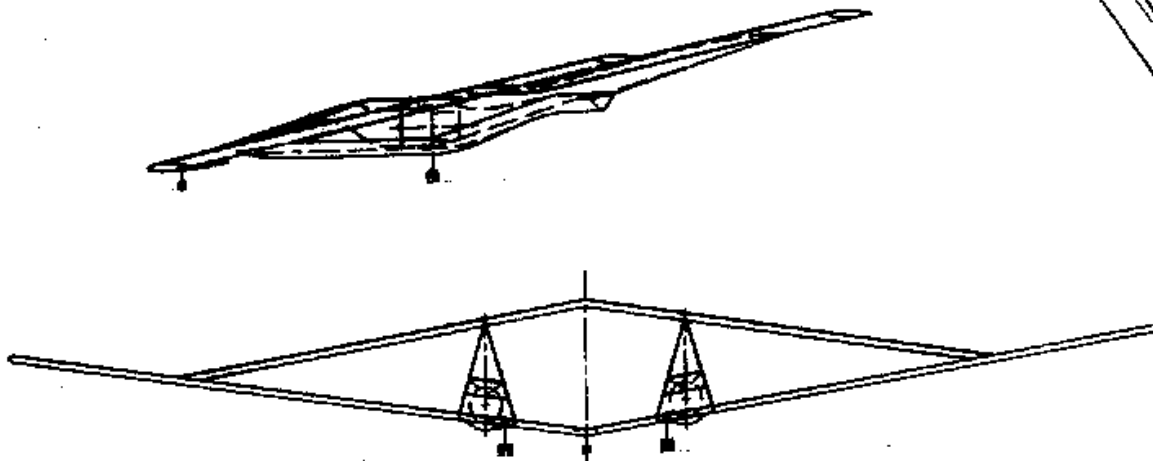
Sweep = 35 deg

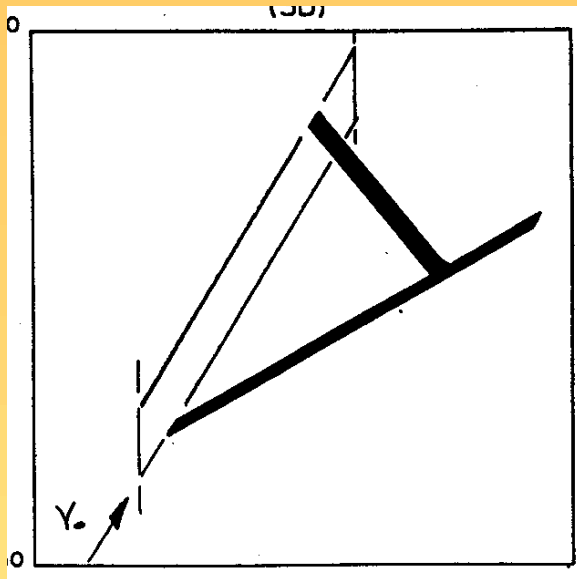


ft

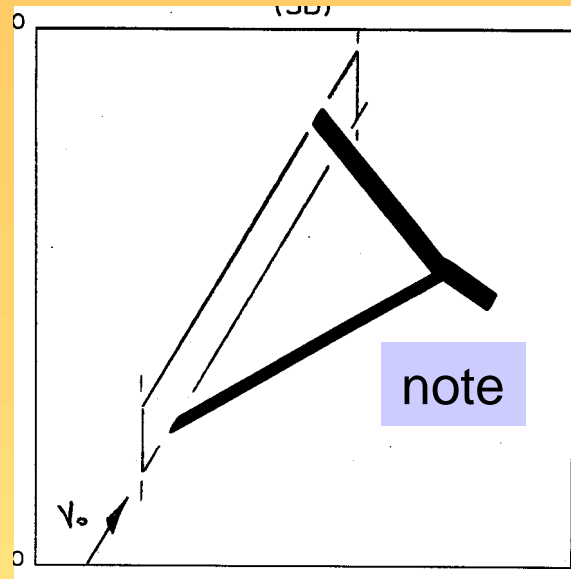


X - Band Antenna

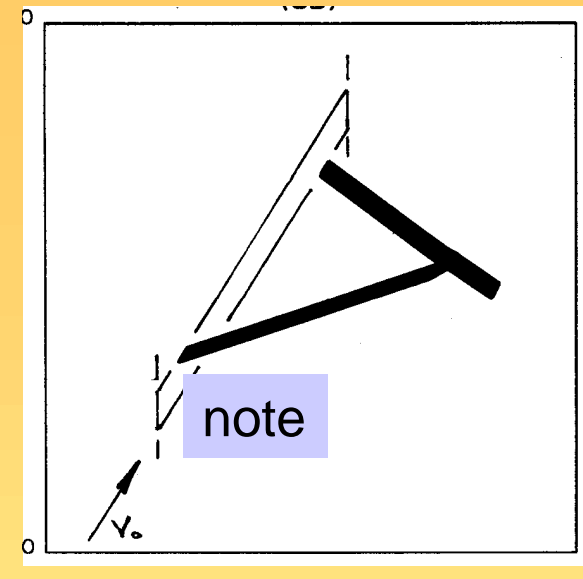




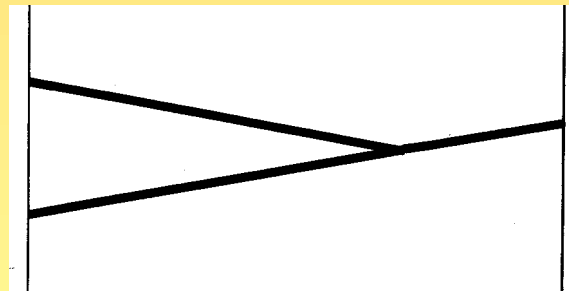
AT1



FT1

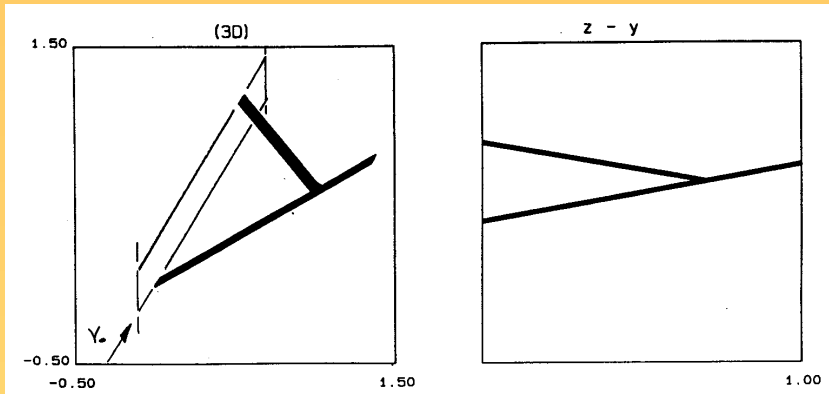


FT2

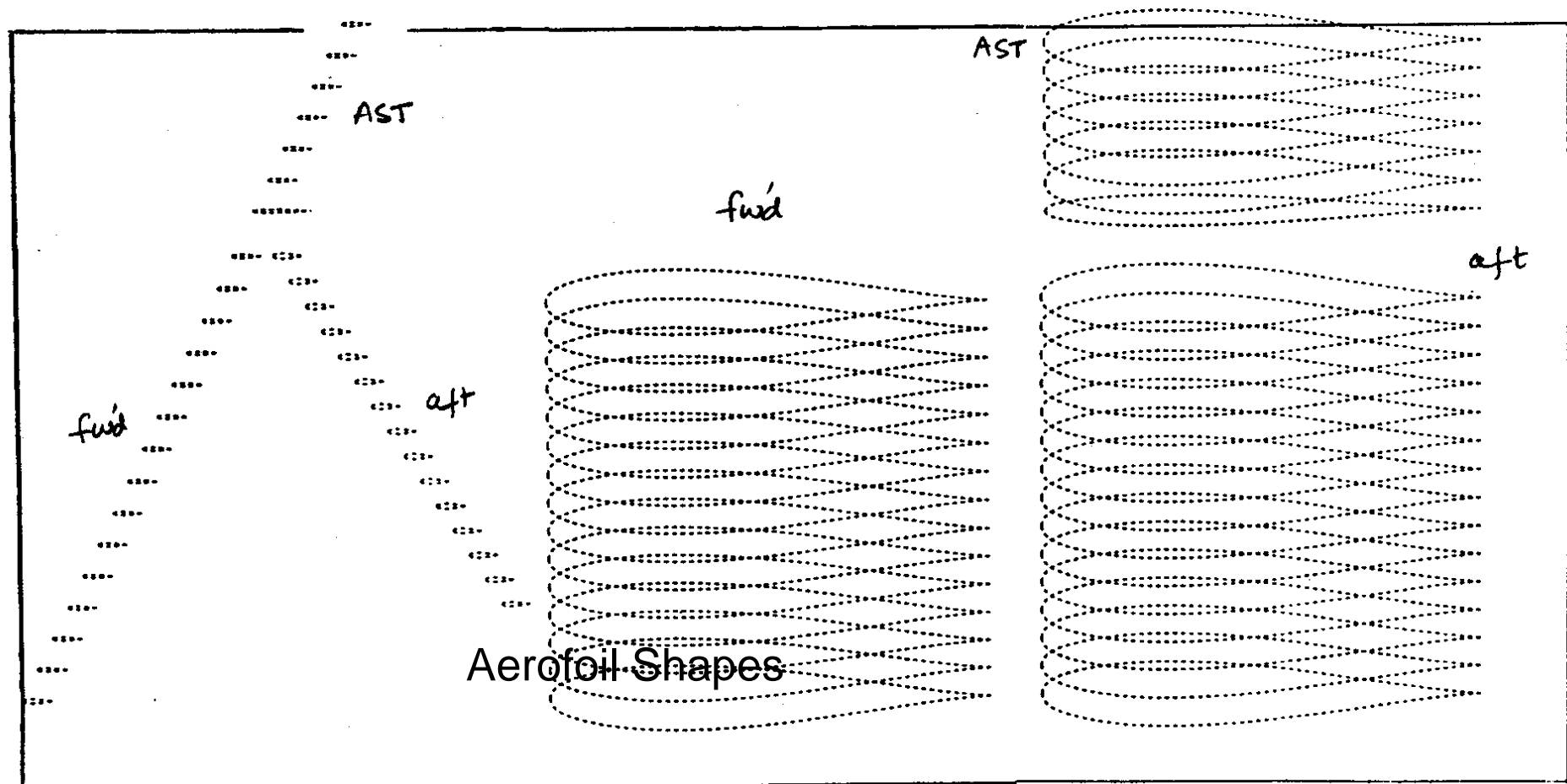


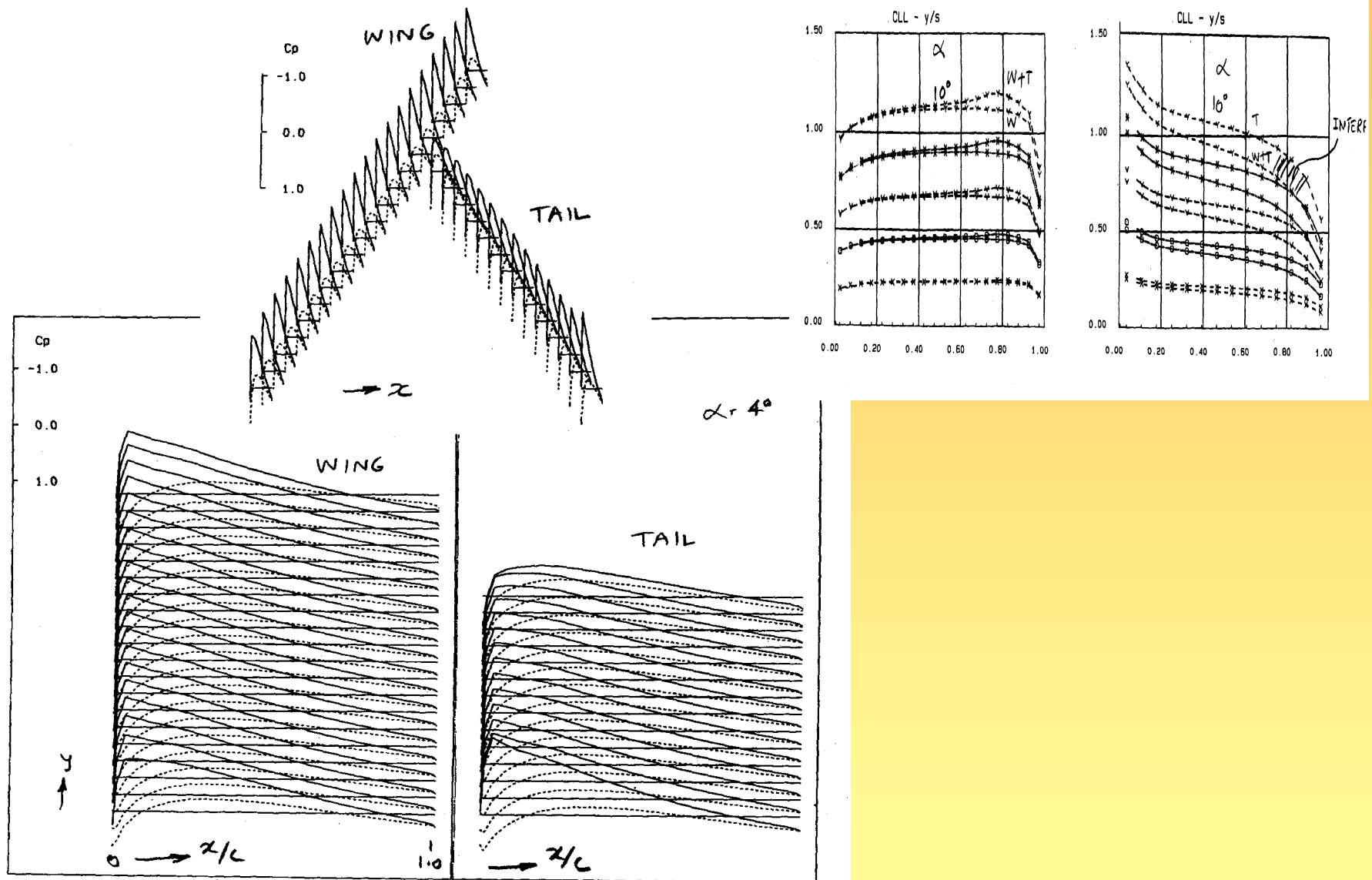
Identical frontal
view

JOINED WING CONFIGURATIONS



AT! CONFIGURATION



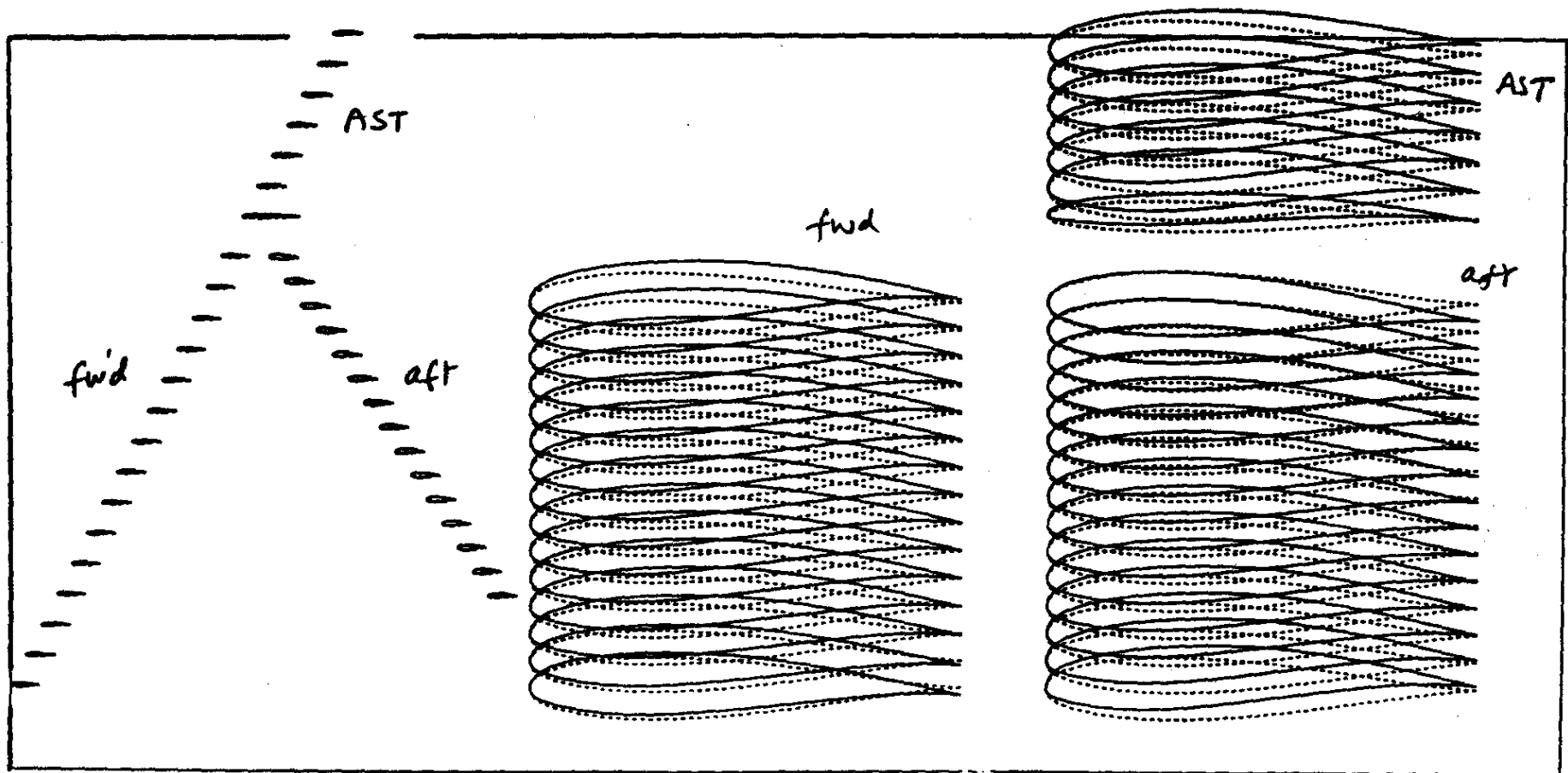


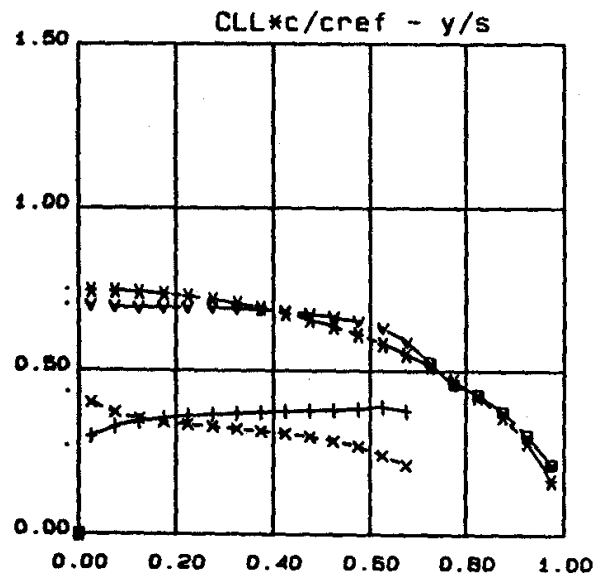
AT!, BASIC CHARACTERISTICS, Uncambered Aerofoils
 Cp Distributions & Interference Effects On Spanwise Loadings

DESIGNED WING, Super-Critical Type Aerofoil, Twist & camber

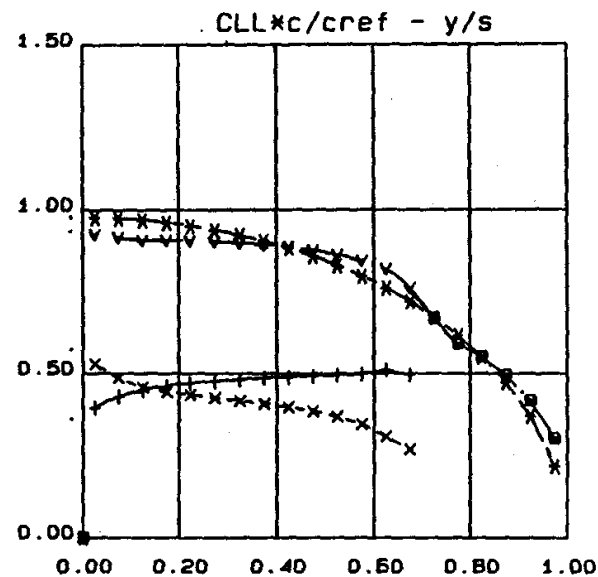
Assume Zero Static Margin (Neutral Stability)

Respective Wing Settings Follow, Use Panel Method

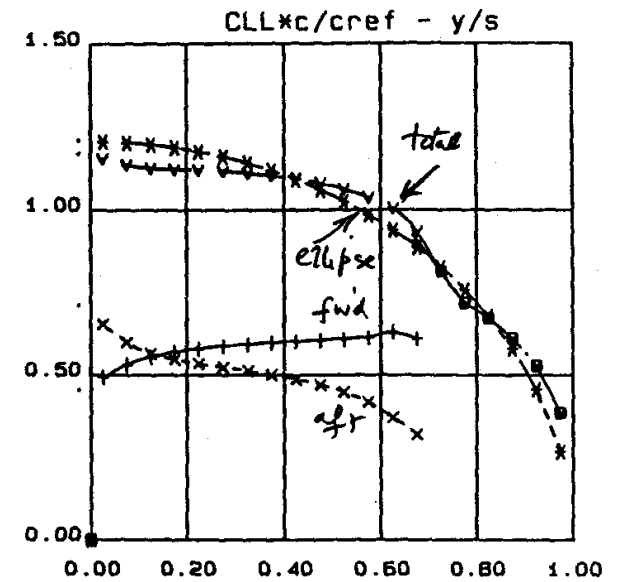




$(\alpha, C_L) = (3.25^\circ, 0.588)$

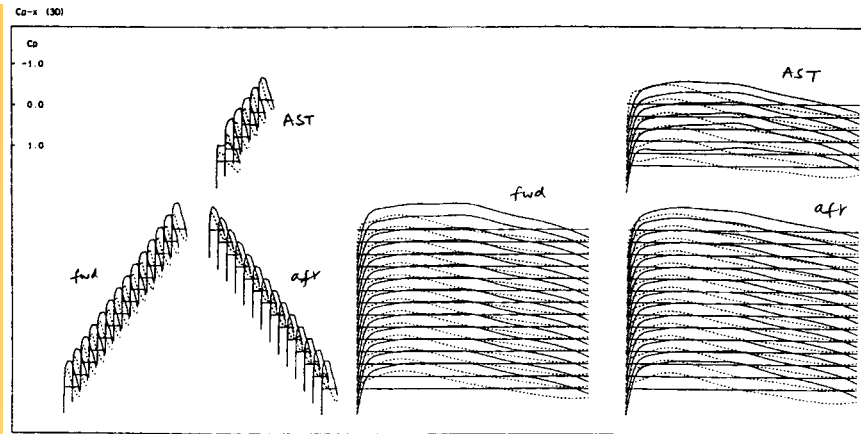


$(\alpha, C_L) = (4.25^\circ, 0.768)$

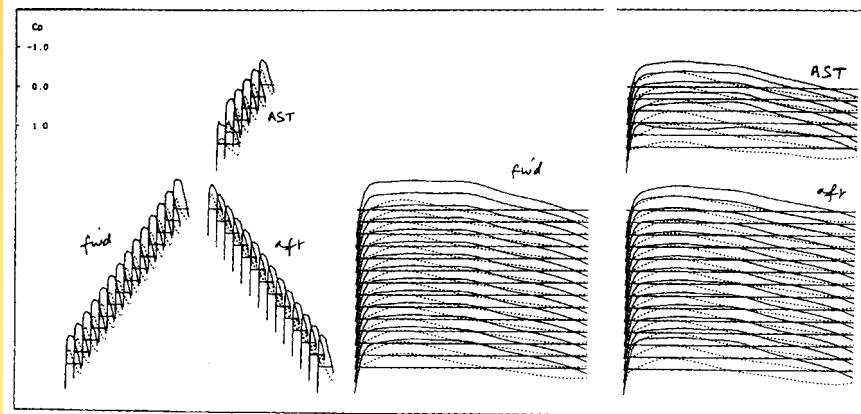


$(\alpha, C_L) = (5.25^\circ, 0.946)$

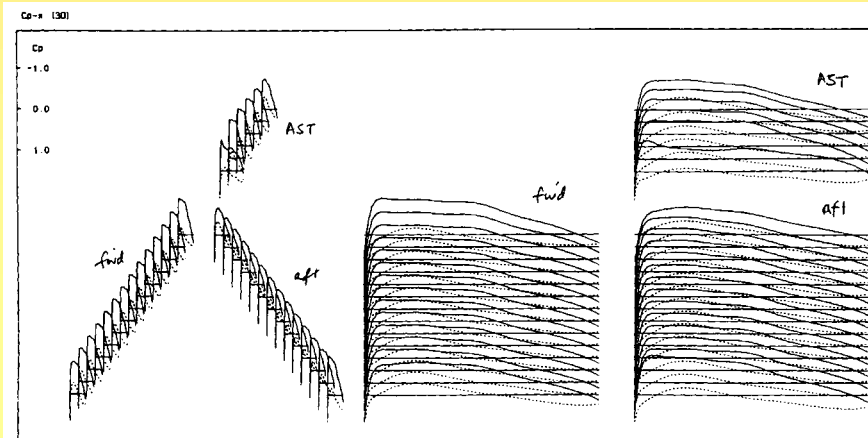
Spanwise Loadings $AoA = 3.25, 4.25, 5.25$



(a) $(\alpha, C_L) = (3.25^\circ, 0.588)$



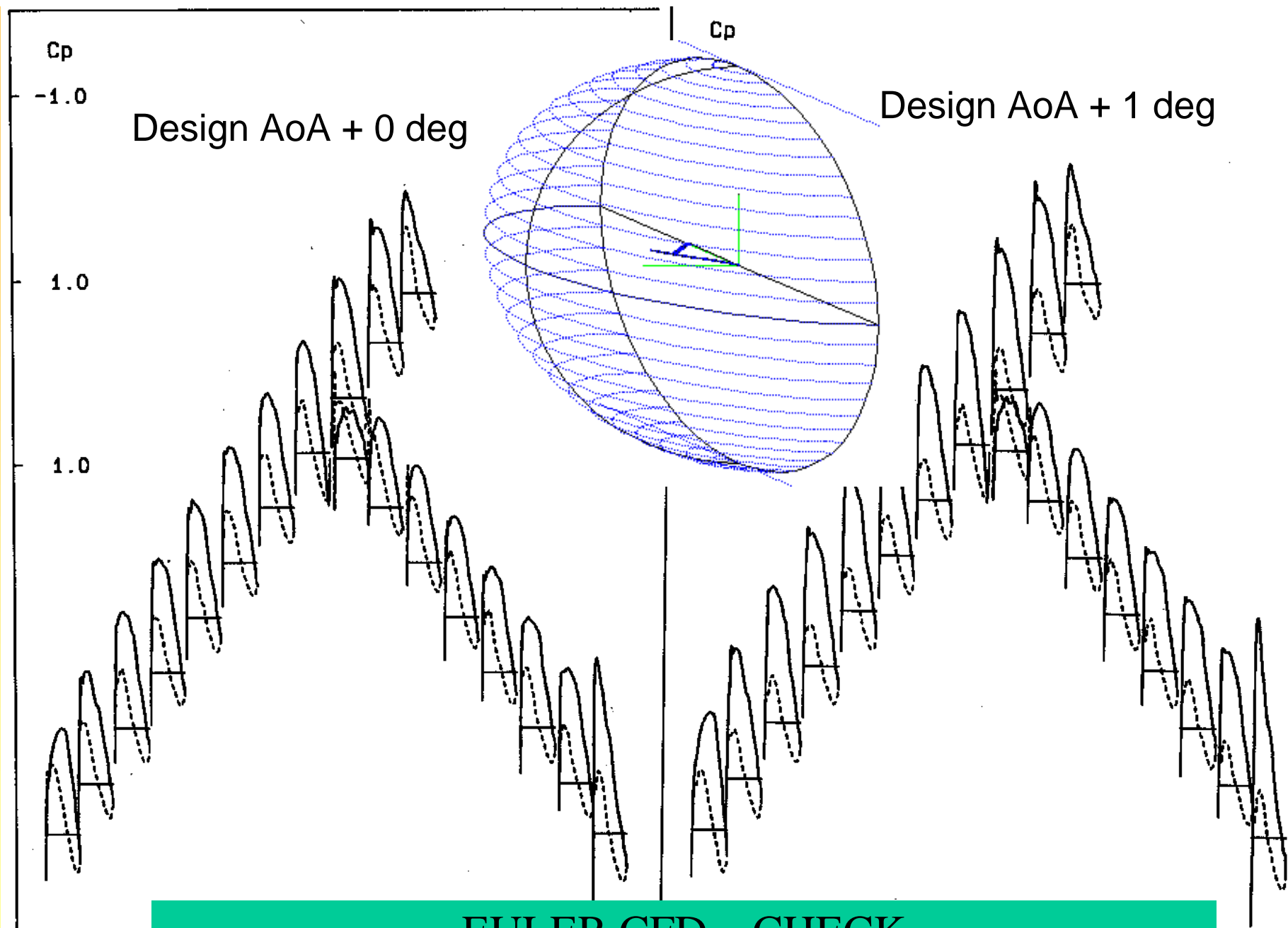
(b) $(\alpha, C_L) = (4.25^\circ, 0.768)$



(c) $(\alpha, C_L) = (5.25^\circ, 0.946)$

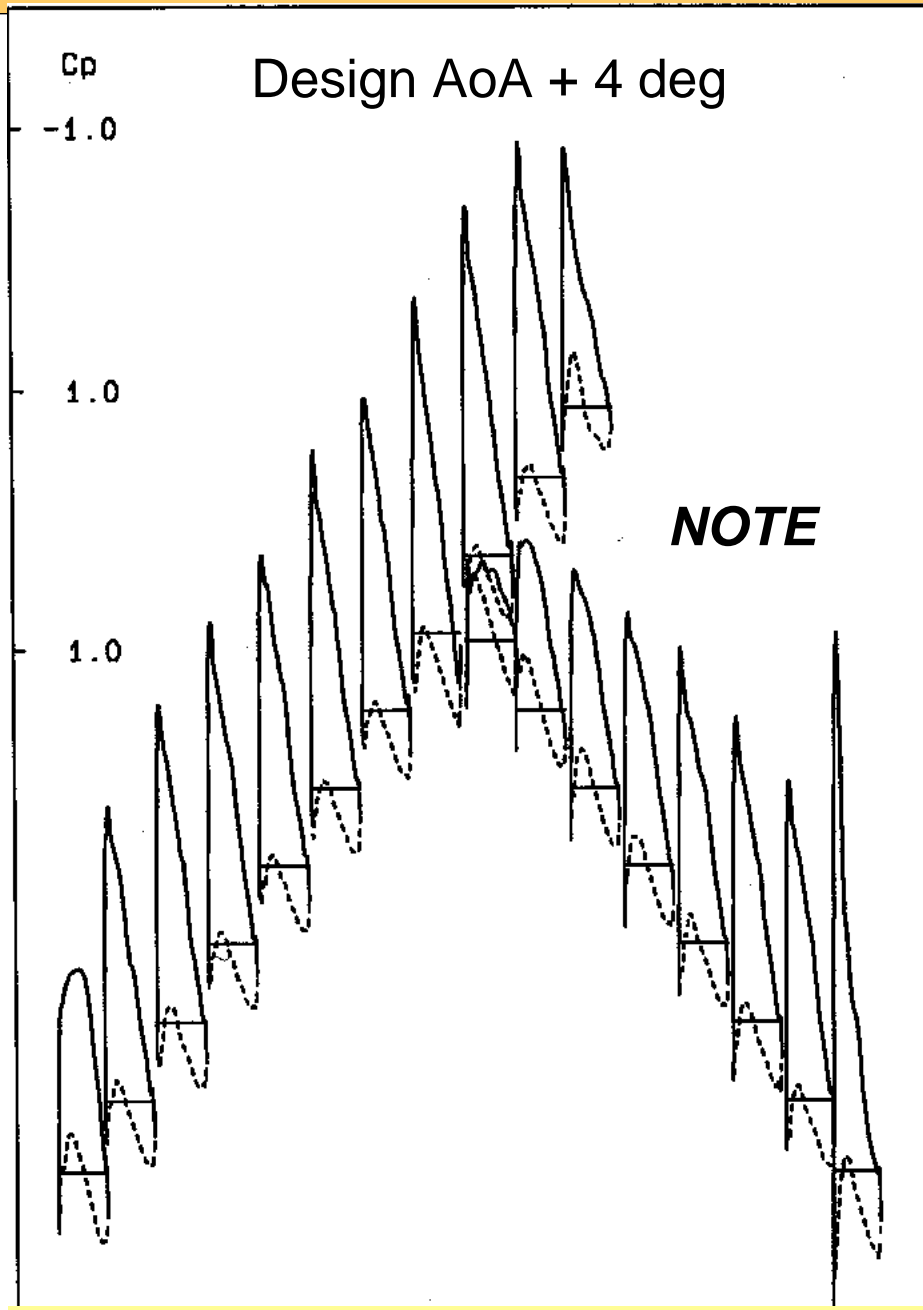
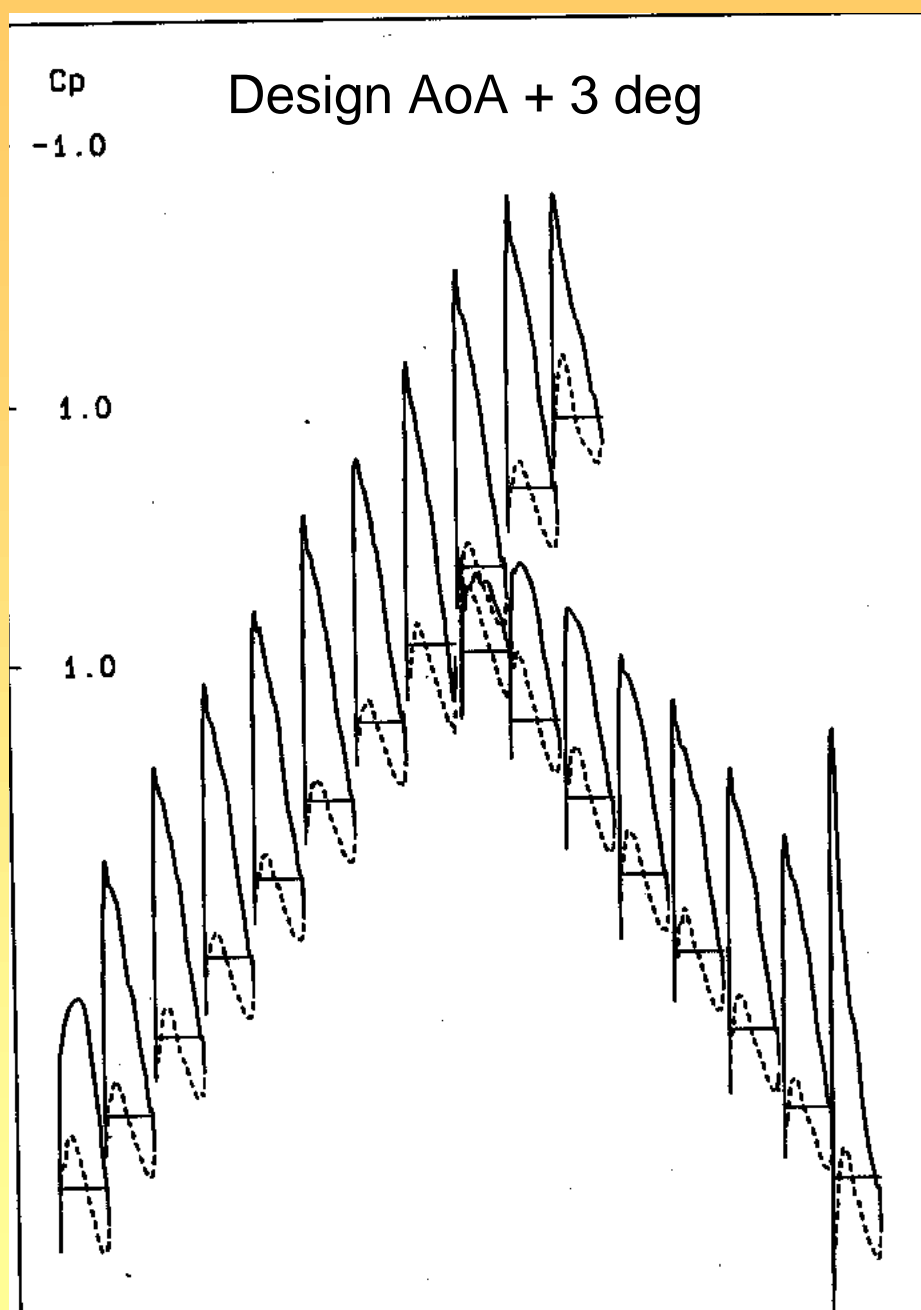
Cp Distbns.

AoA = 3.25, 4.25, 5.25



EULER CFD CHECK

Designed Case & Off-Design look for extreme gradients



Cd-x (30)

Cp

Panel, CL = 0.59

-1.0

0.0

1.0

AST

fwl

afx

Cp

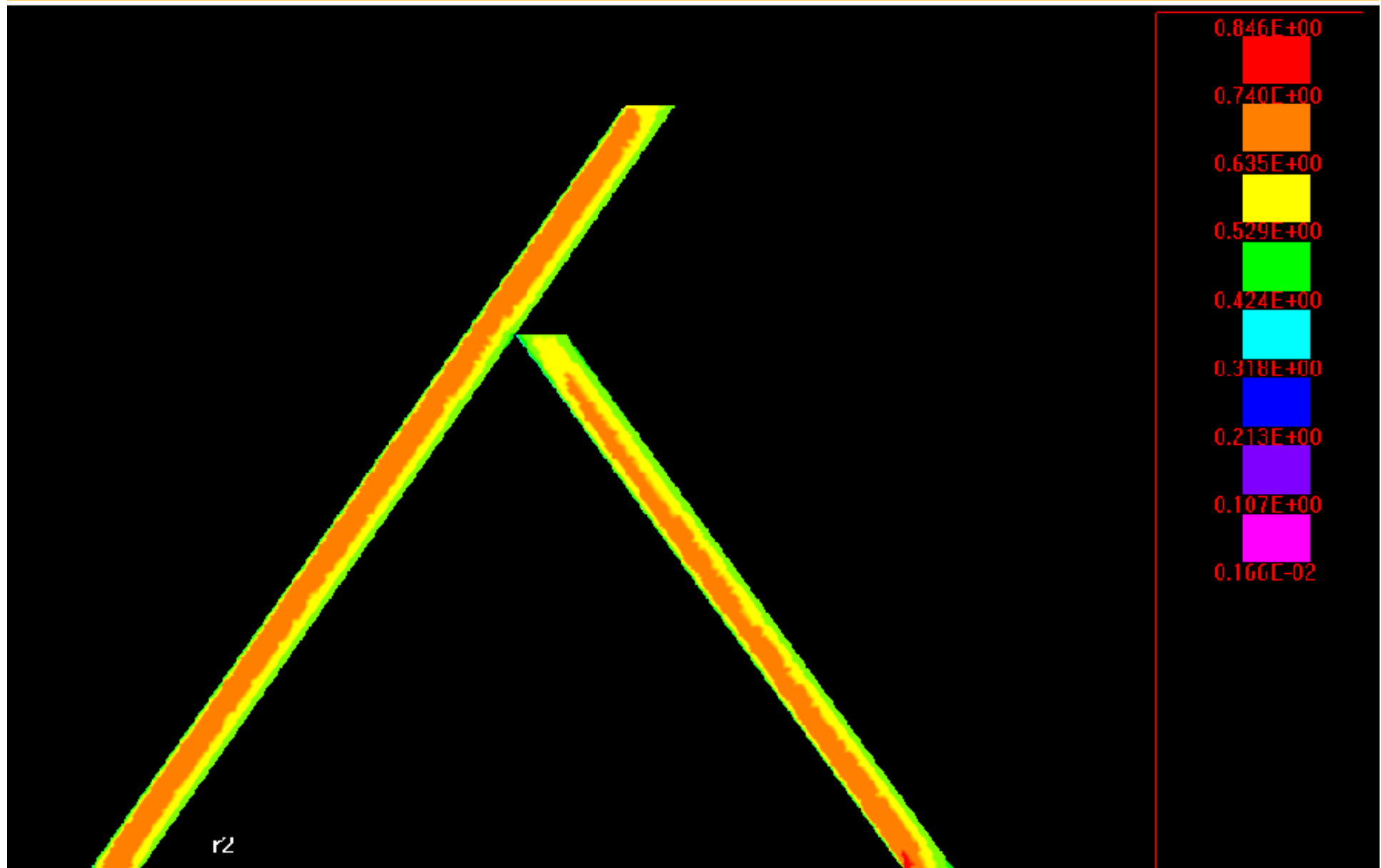
-1.0

Euler, CL = 0.51

1.0

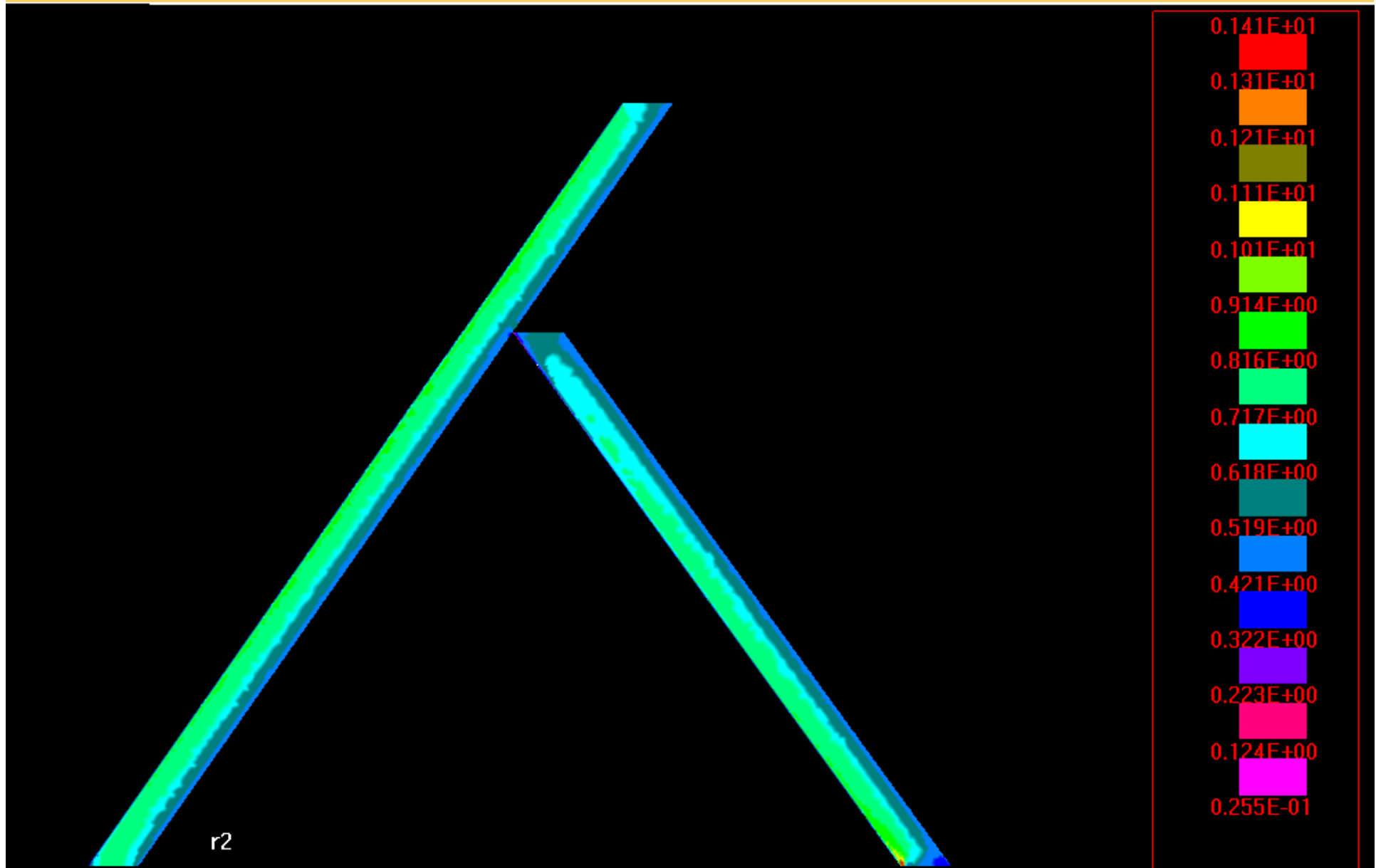
1.0

Mach no



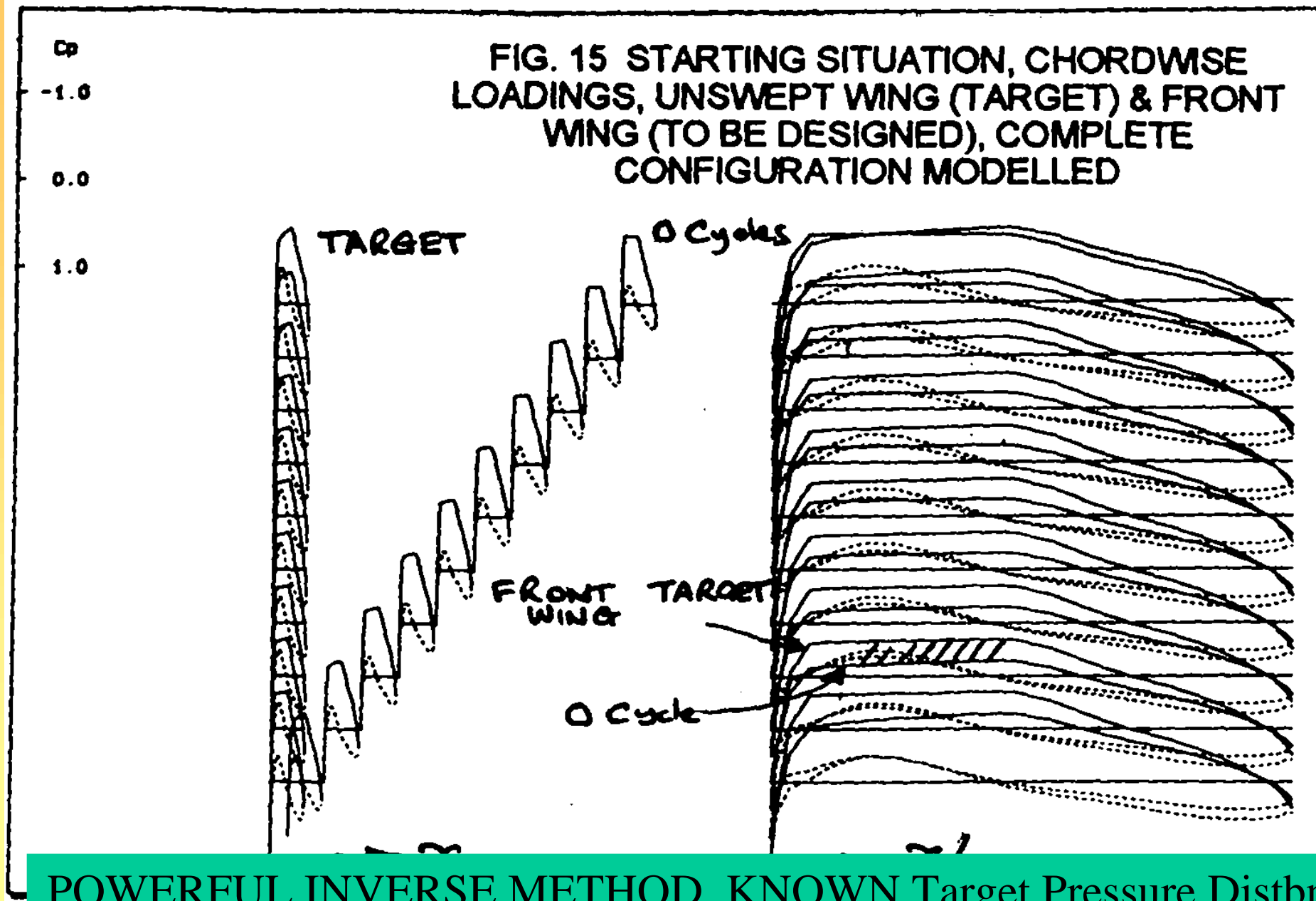
Euler, M=0.6, Design AoA + 0 deg, CL = 0.51, Upper Surface

Mach no.



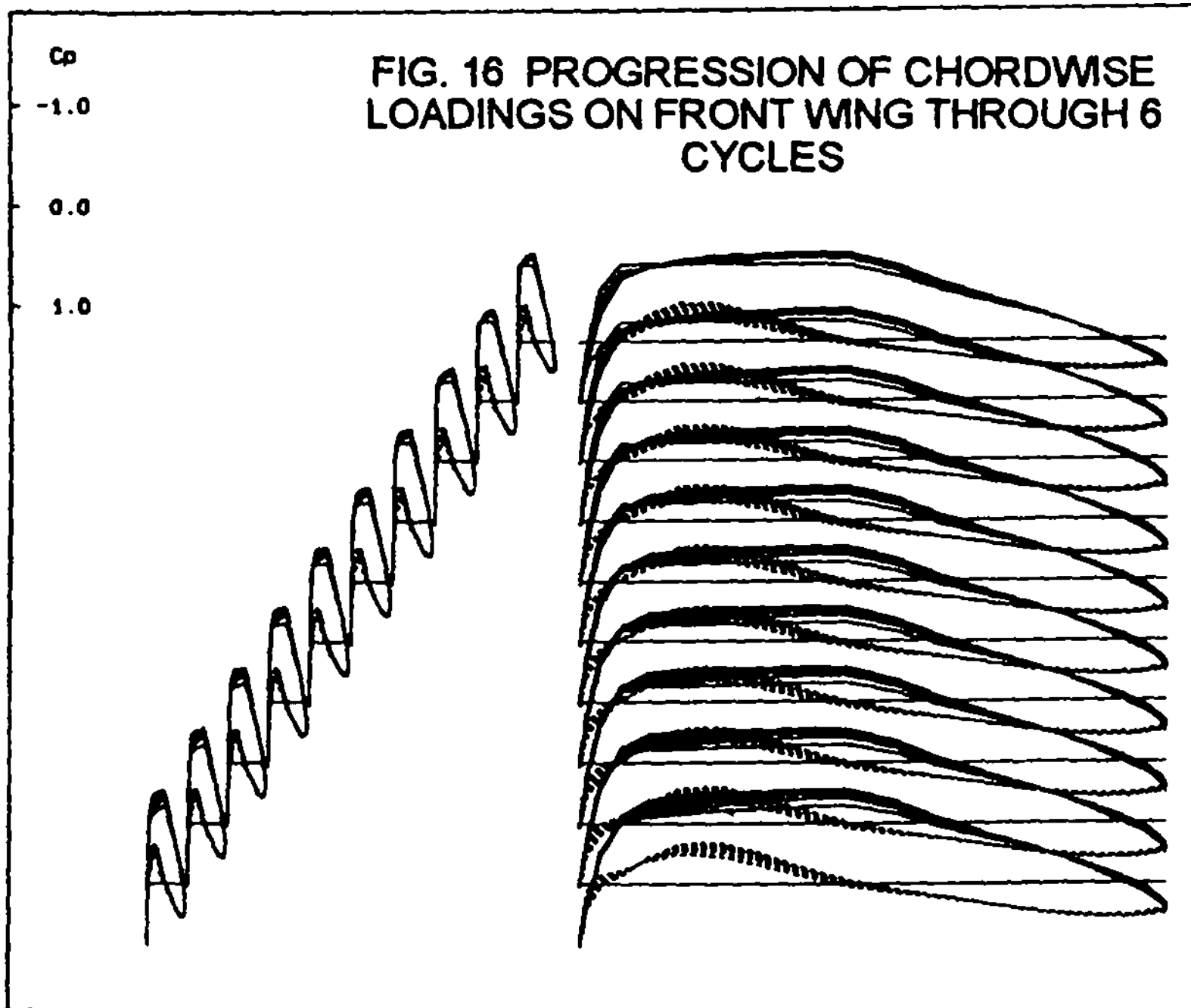
Euler, M=0.6, Design AoA + 4 deg, CL = 1.08, Upper Surface

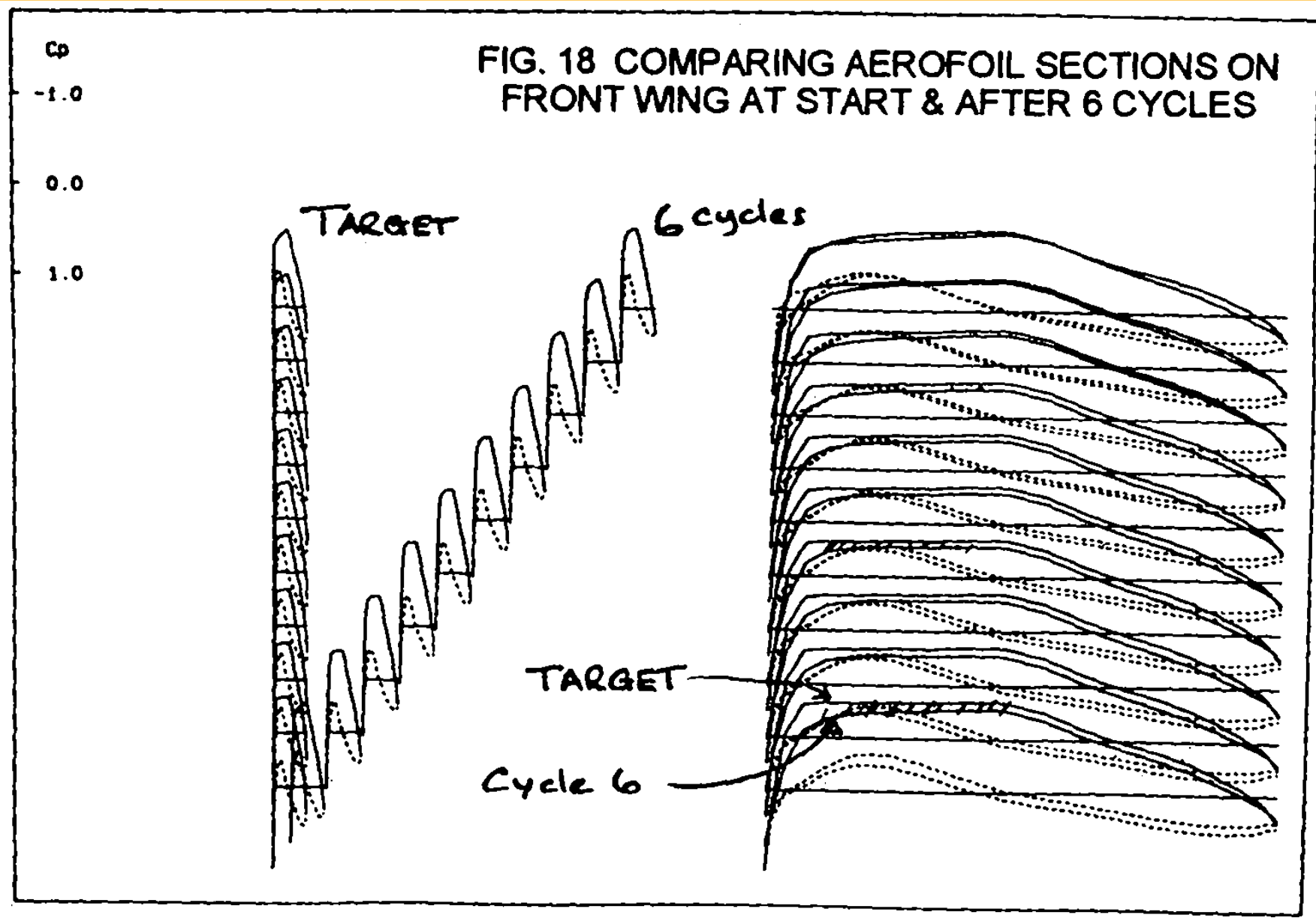
FIG. 15 STARTING SITUATION, CHORDWISE LOADINGS, UNSWEPT WING (TARGET) & FRONT WING (TO BE DESIGNED), COMPLETE CONFIGURATION MODELLED



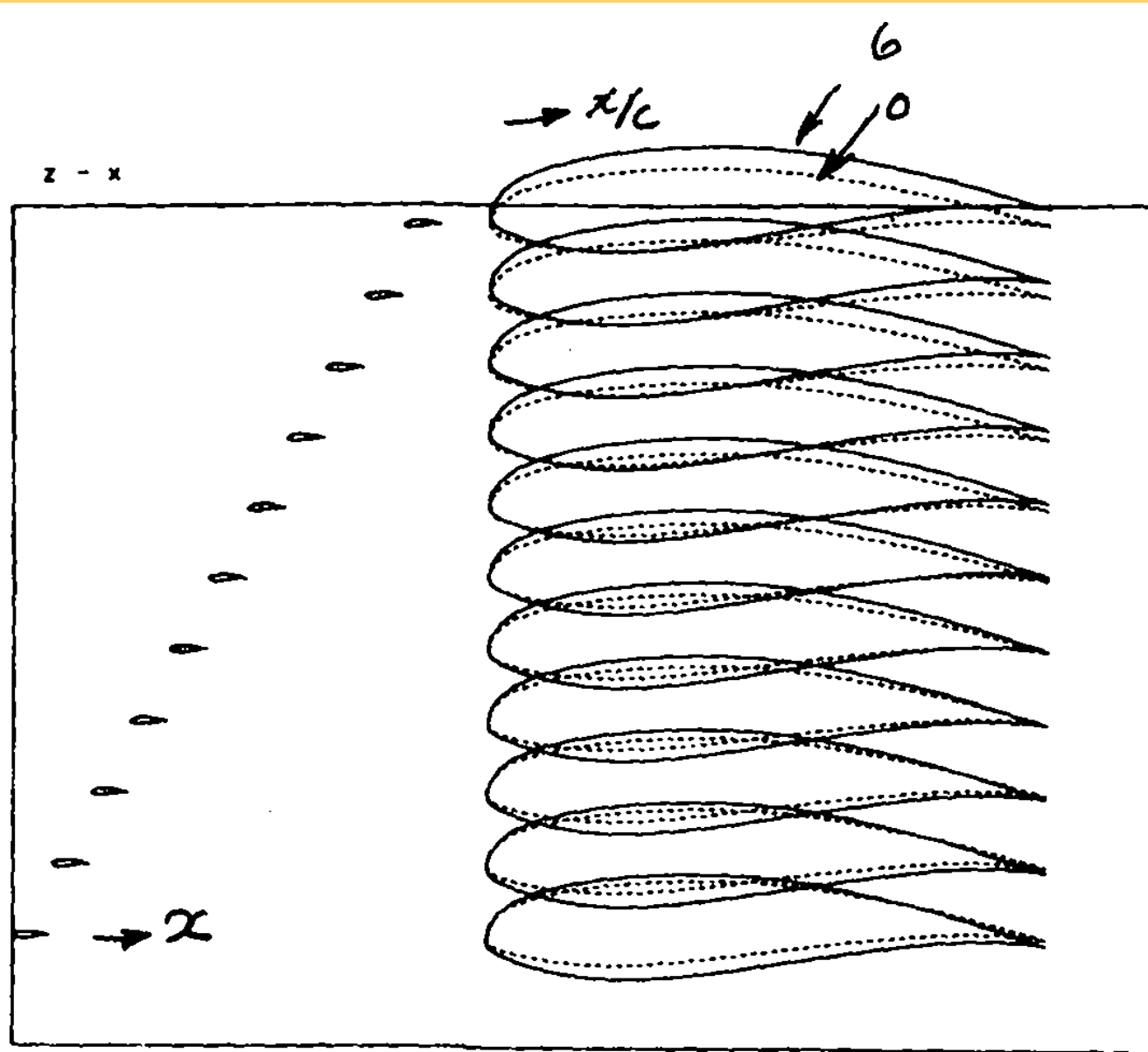
POWERFUL INVERSE METHOD, KNOWN Target Pressure Distbn.
 "Supplanted" on a GIVEN WING

FIG. 16 PROGRESSION OF CHORDWISE
LOADINGS ON FRONT WING THROUGH 6
CYCLES

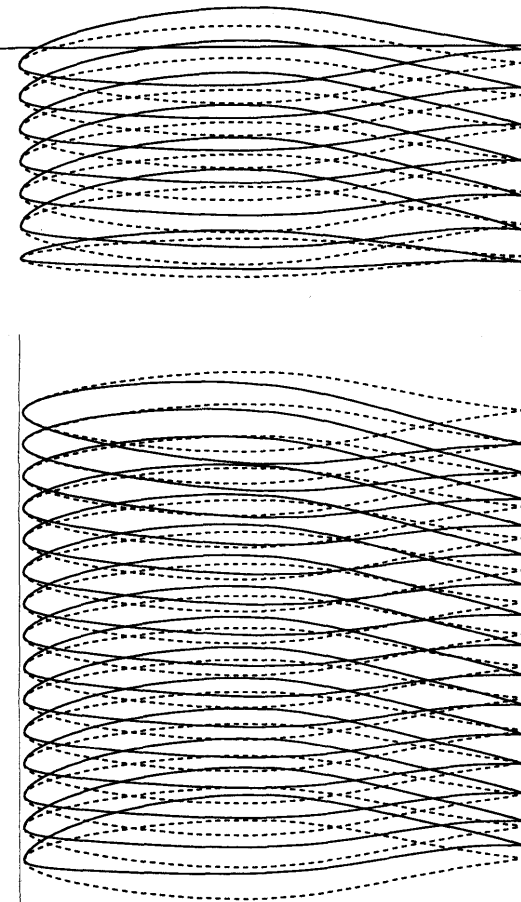
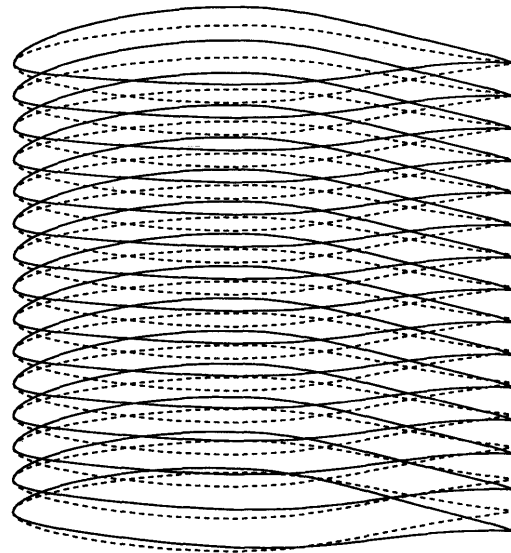
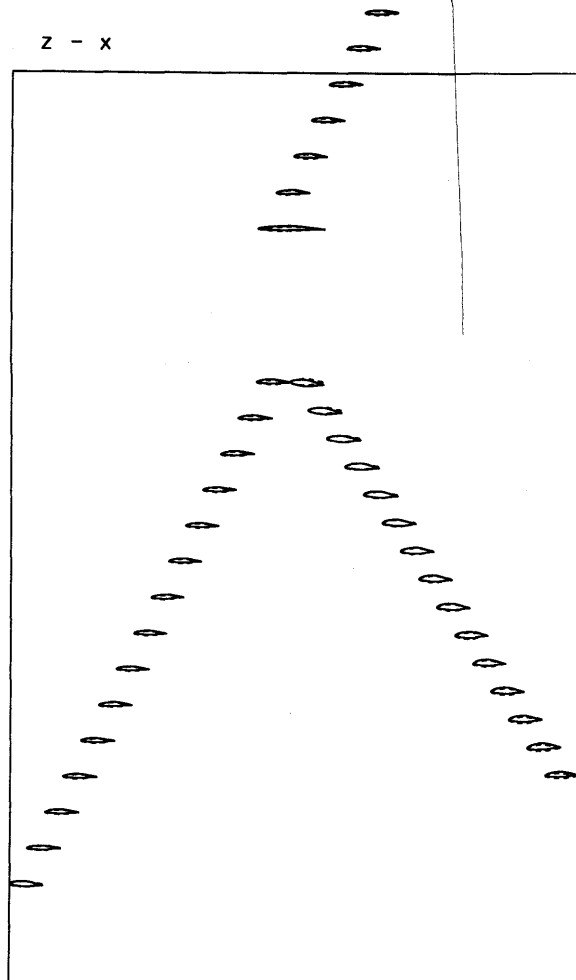
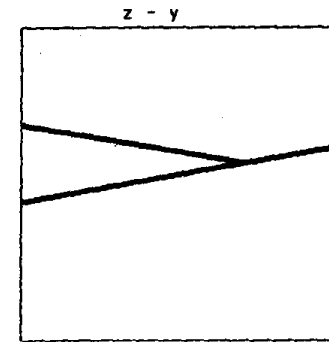
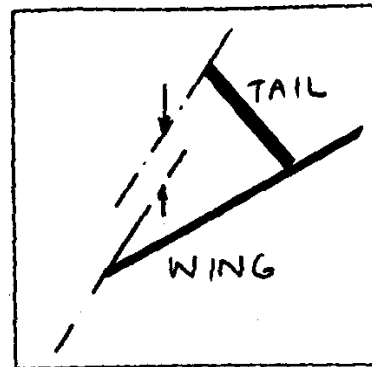


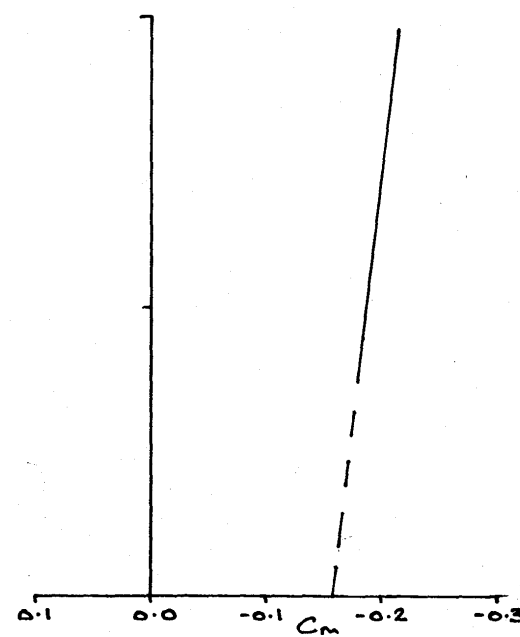
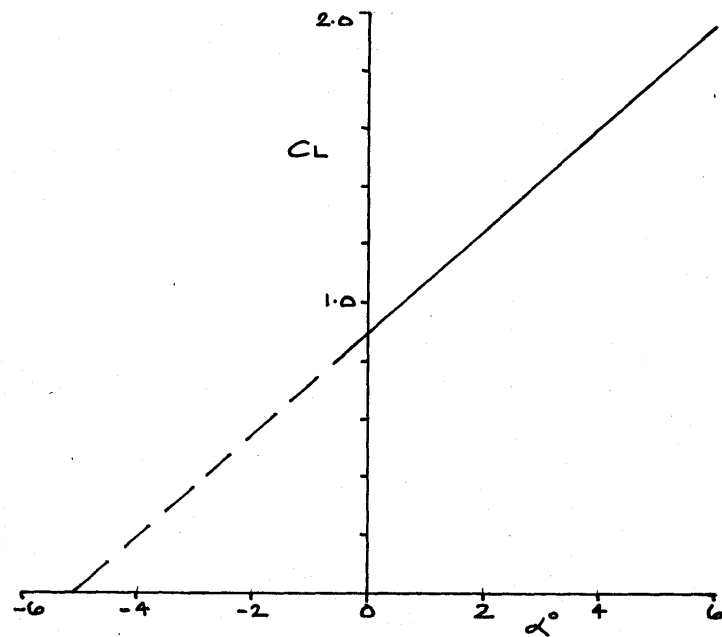


COMPARING AEROFOIL SECTIONS ON FRONT WING AT START & AFTER 6 CYCLES (WING AND TAIL BOTH MODELLED)

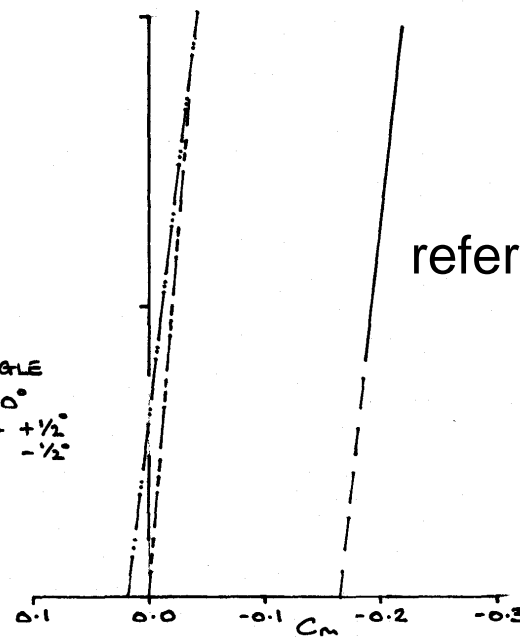
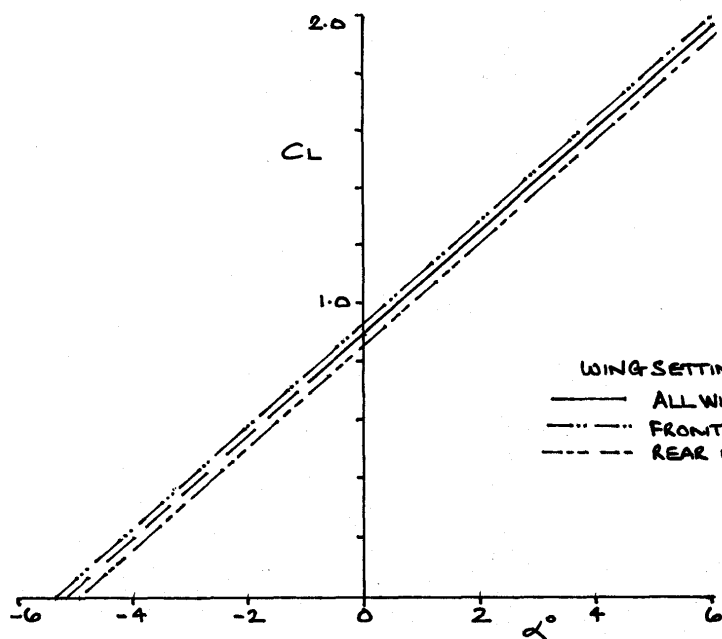


Laminar AT1

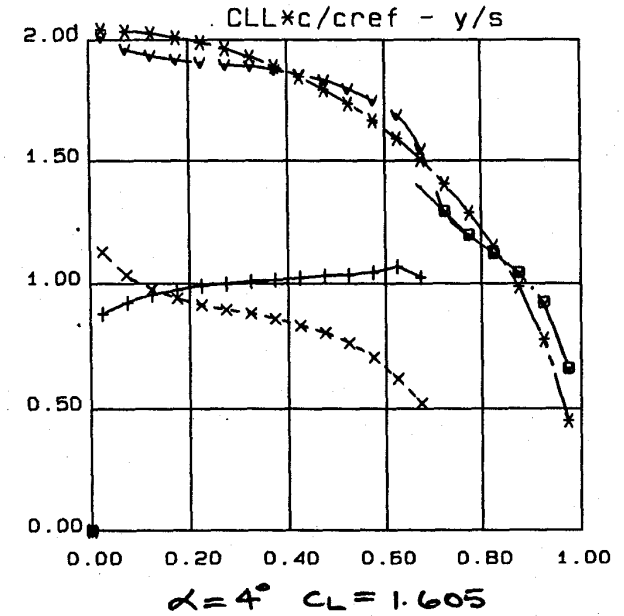
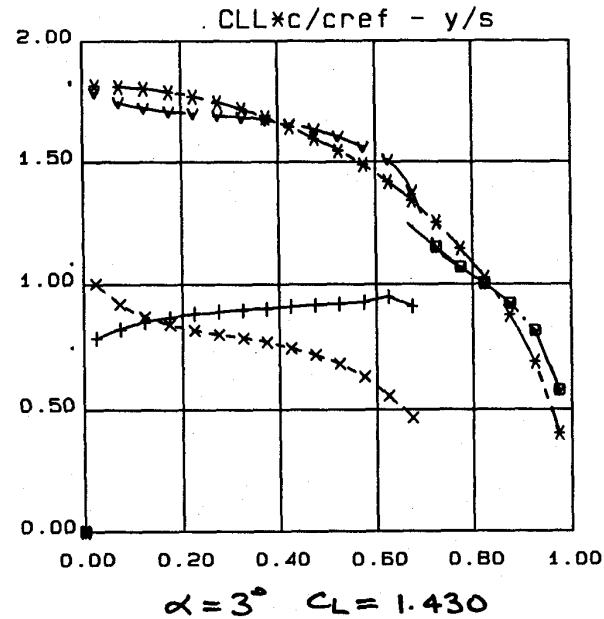
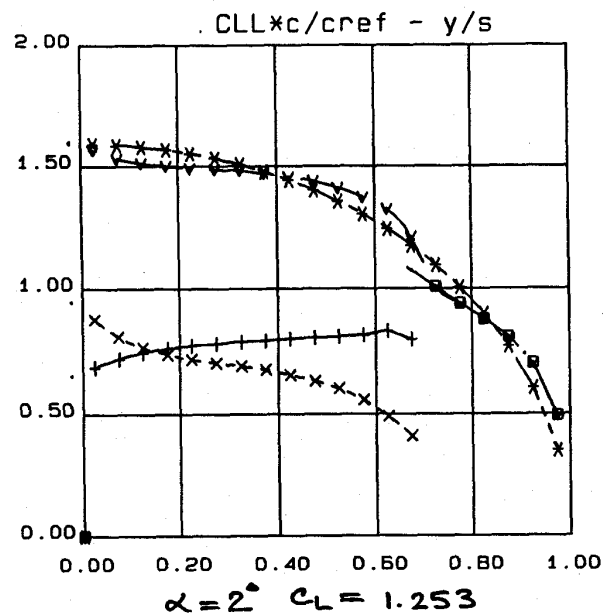
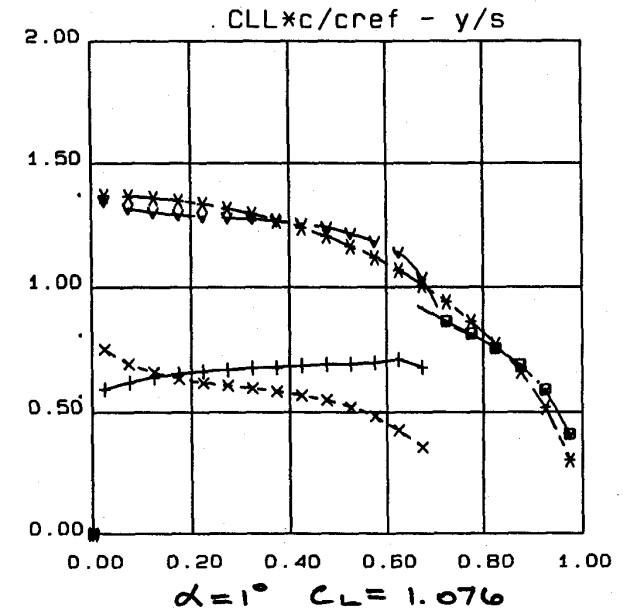
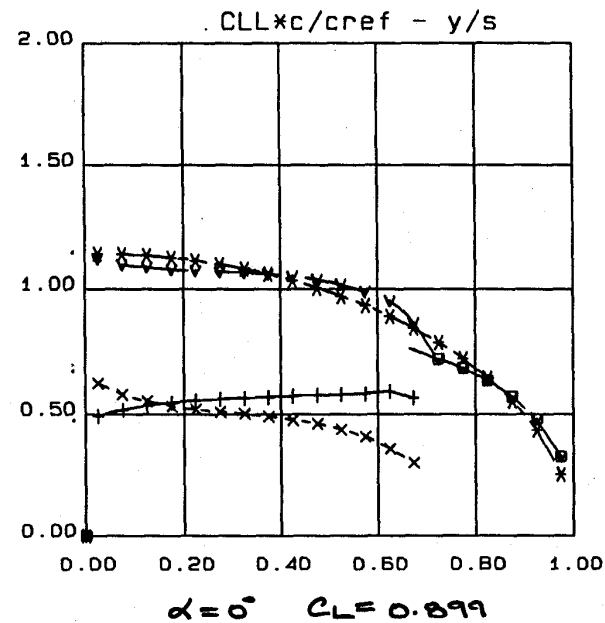
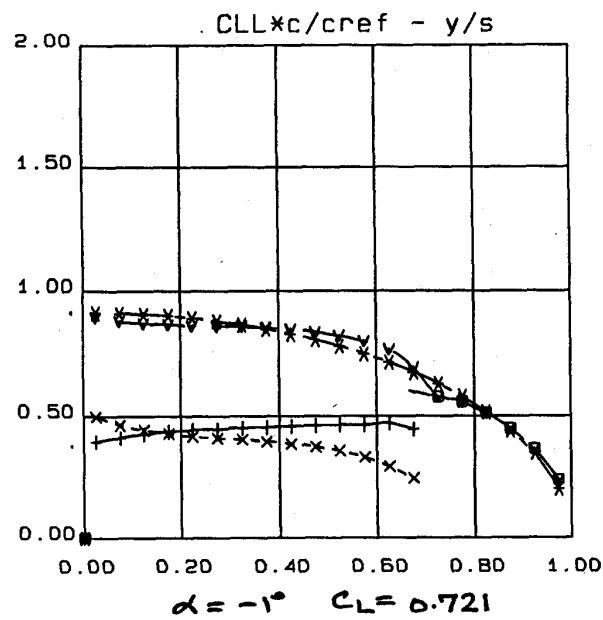




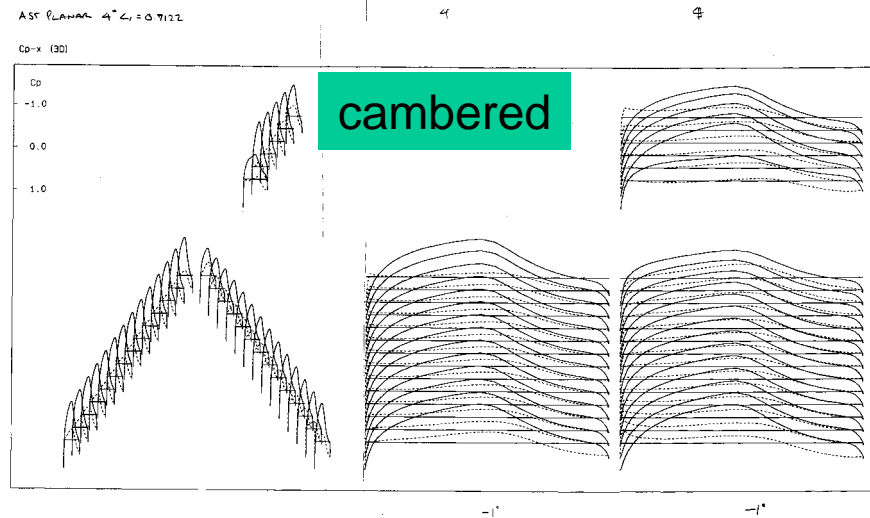
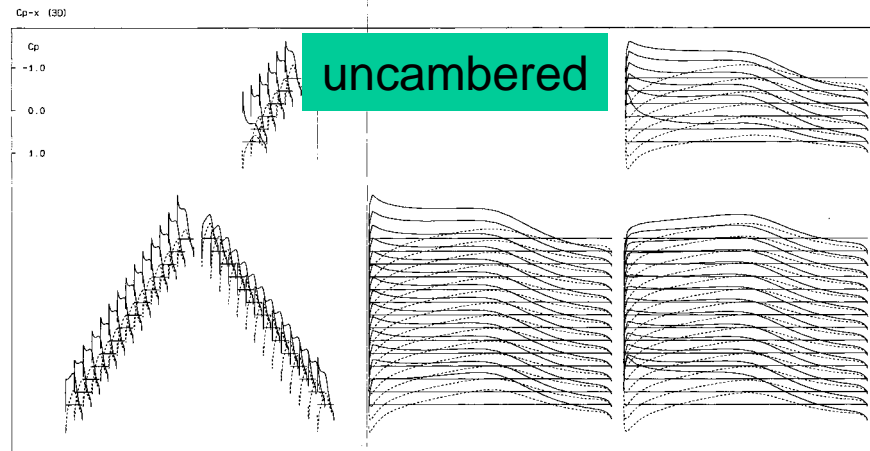
CL & Cm
Reference &
Control due to 0.5
deg setting angle
changes



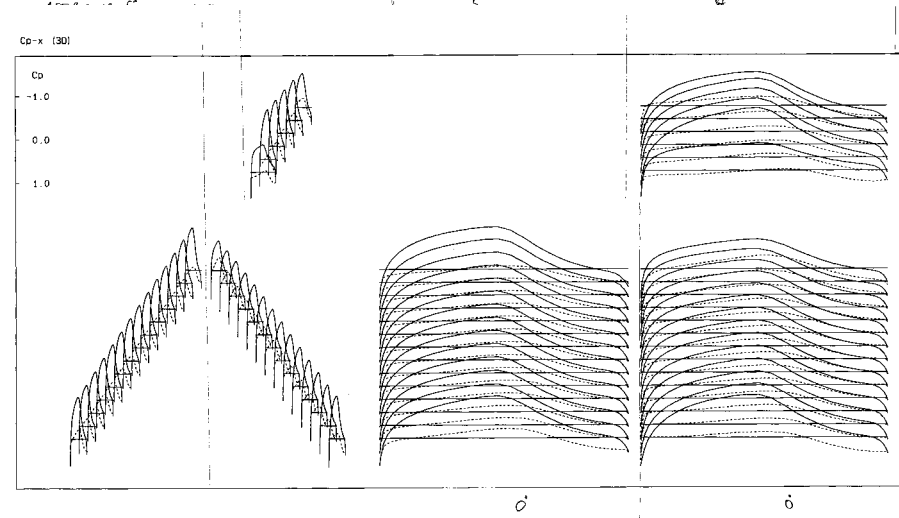
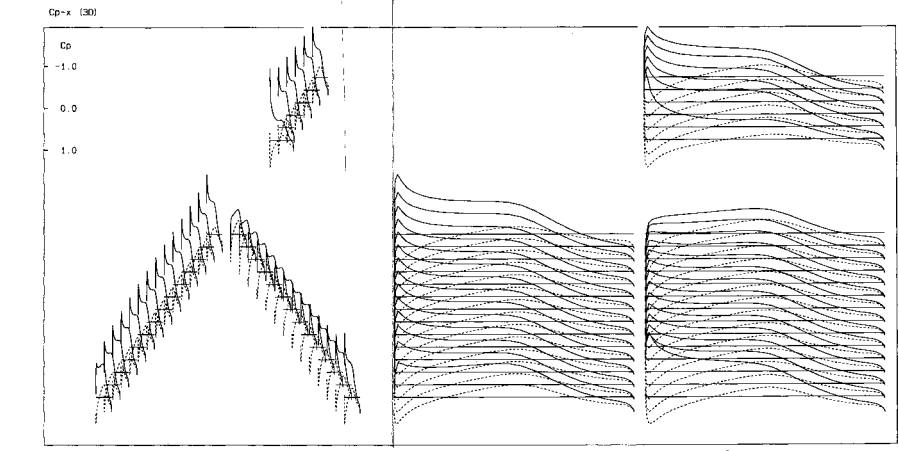
reference



SPANWISE LOADINGS AT Mach 0.6, $C_L = 0.72, 0.9, 1.07, 1.25, 1.43, 1.6$

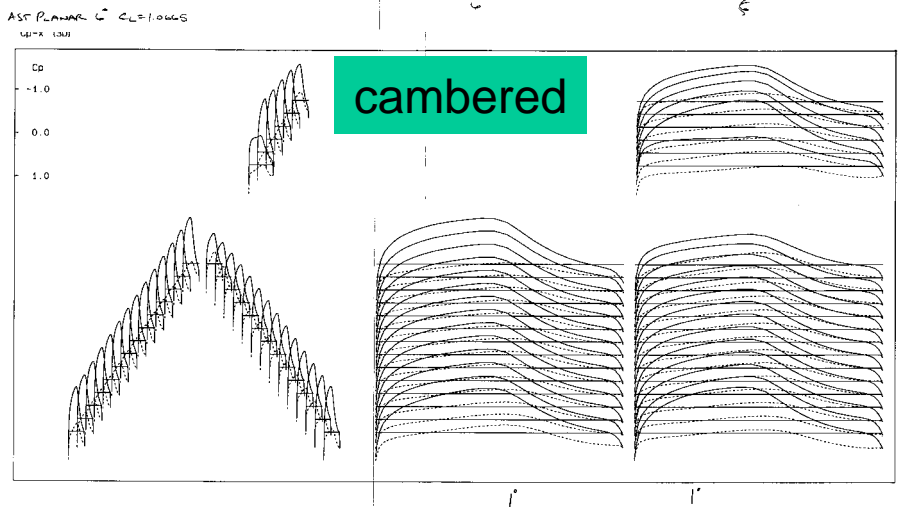
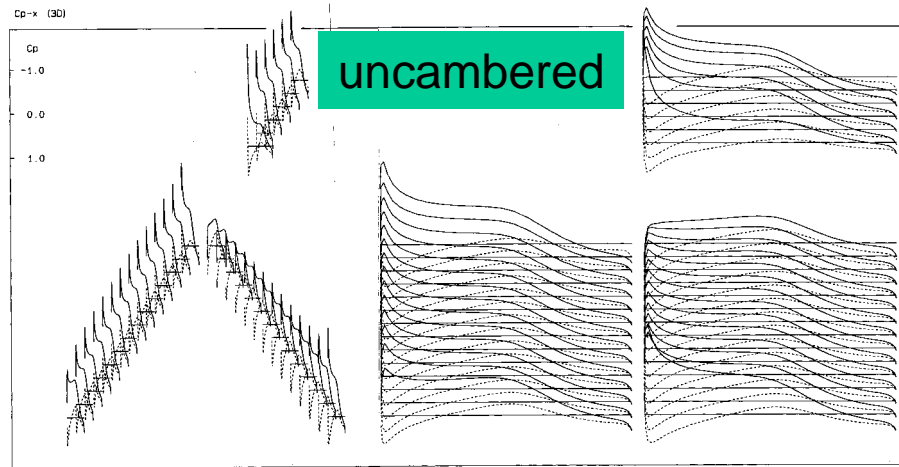


CL=0.72

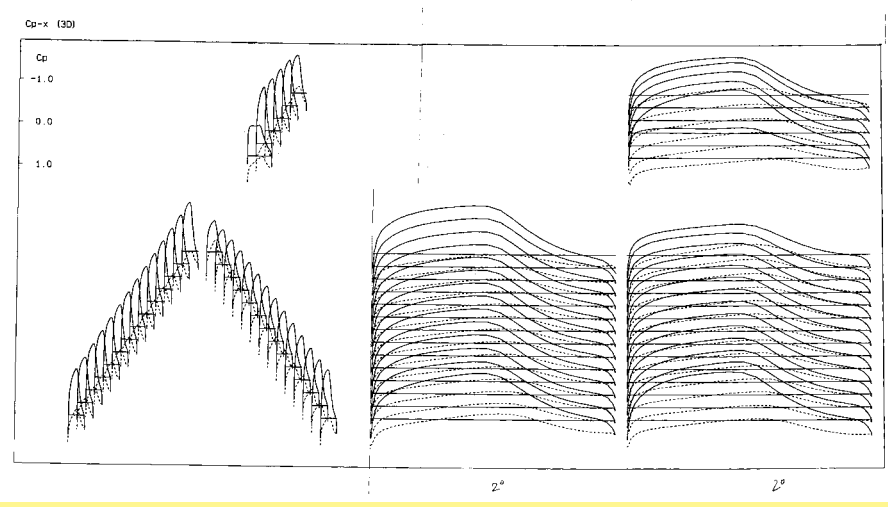
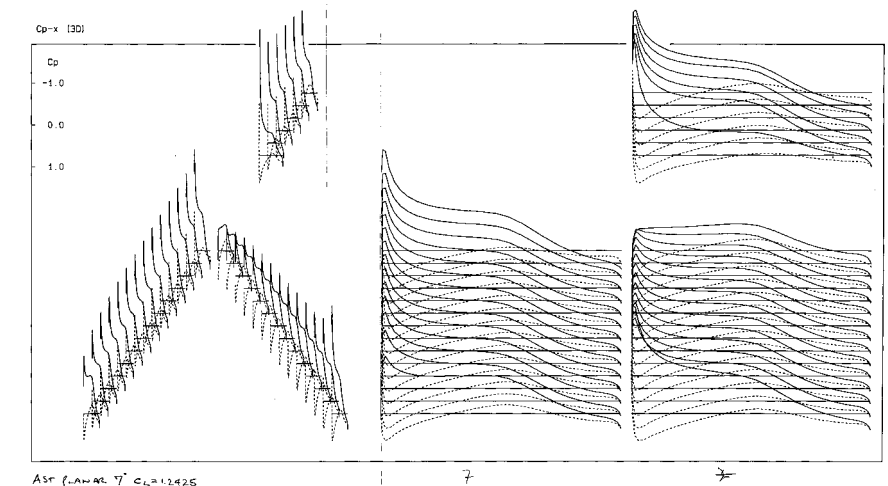


CL=0.9

COMPARING UNCAMBERED & DESIGNED CONFIGS AT
SAME CL VALUES

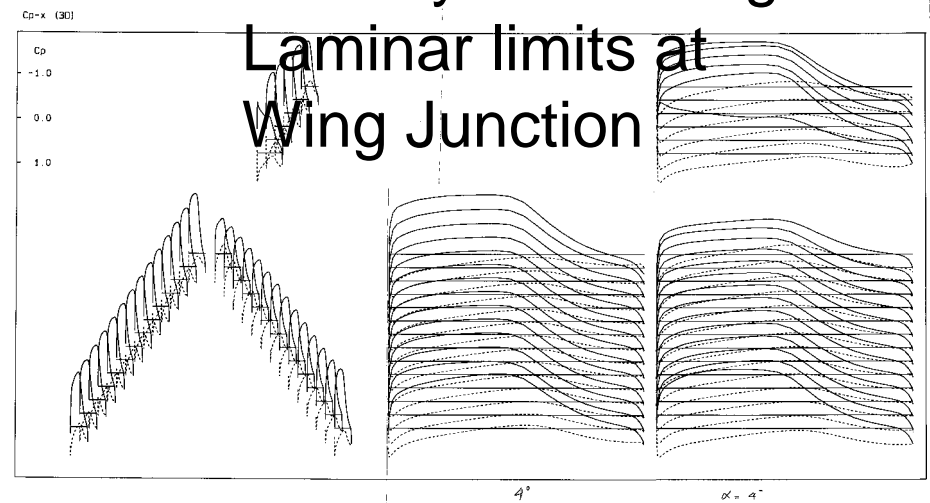
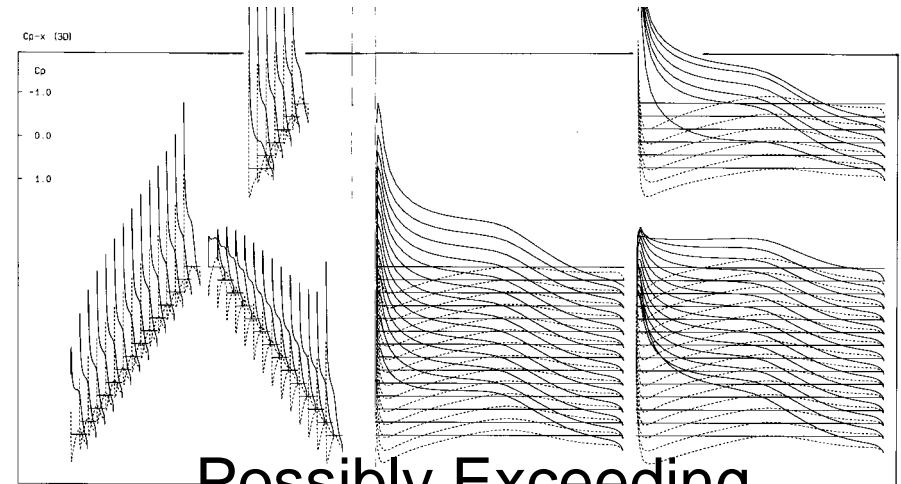
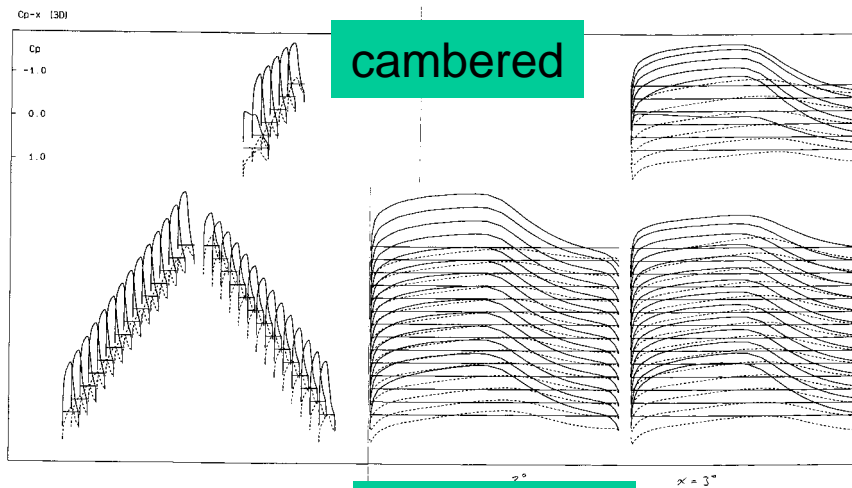
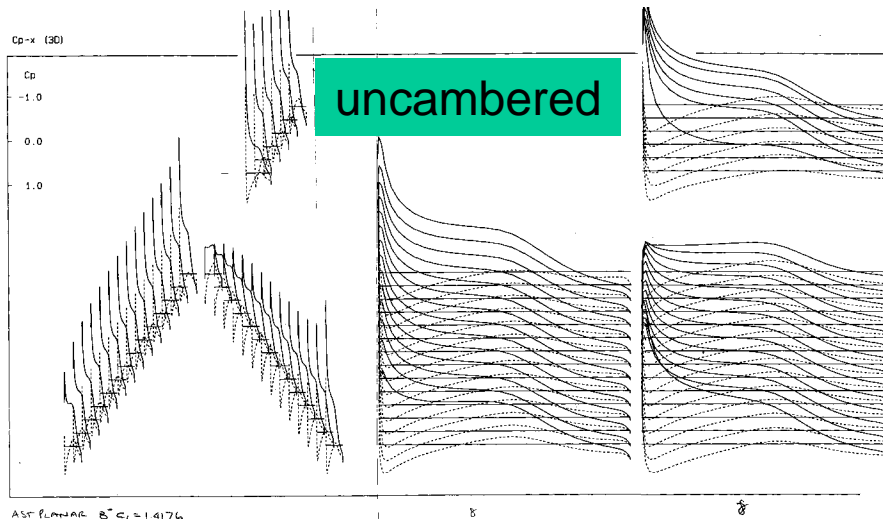


CL=1.07

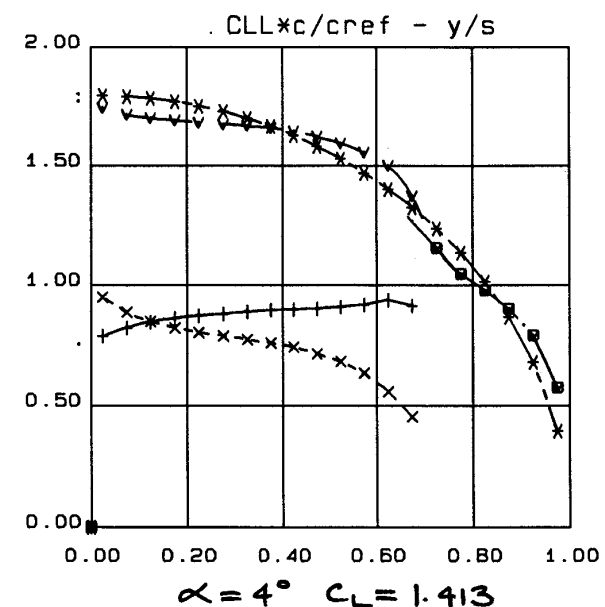
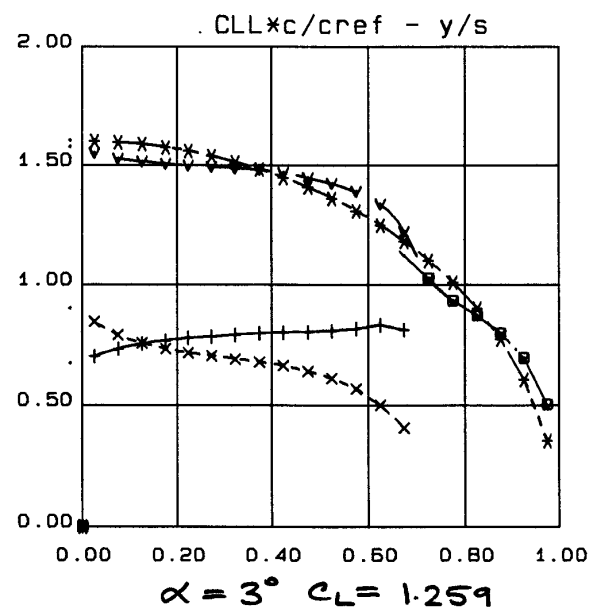
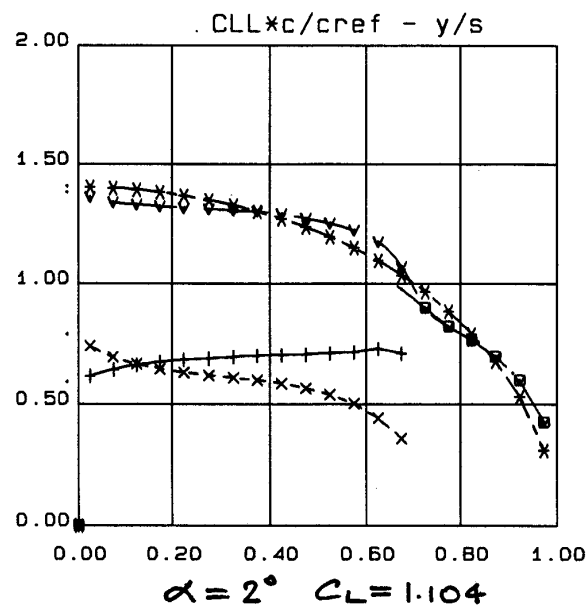
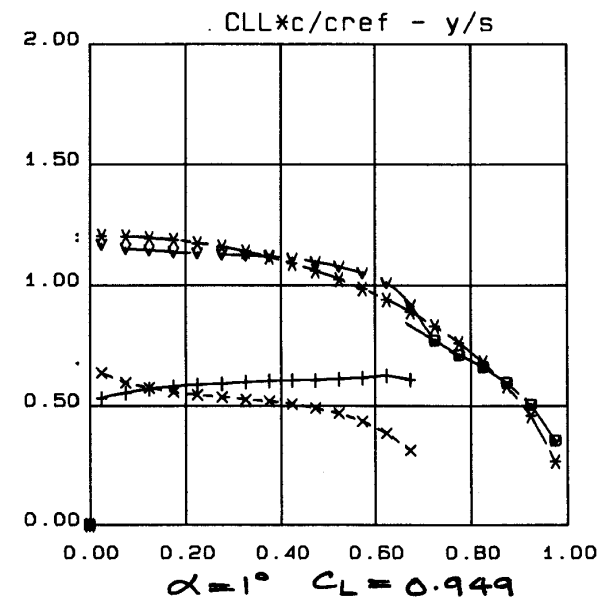
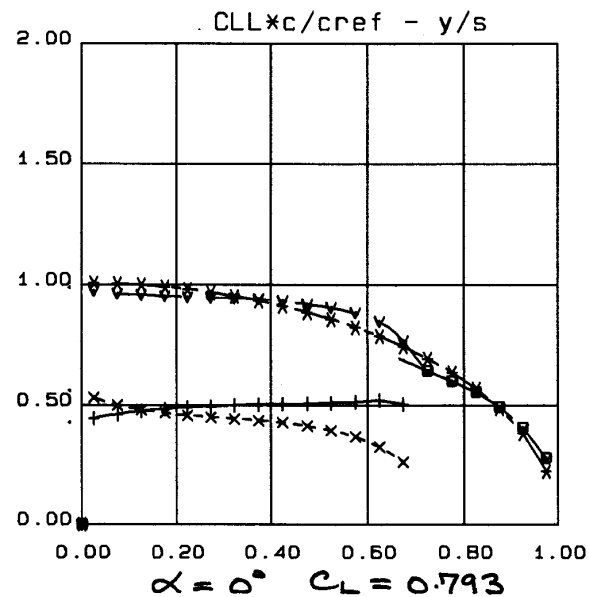
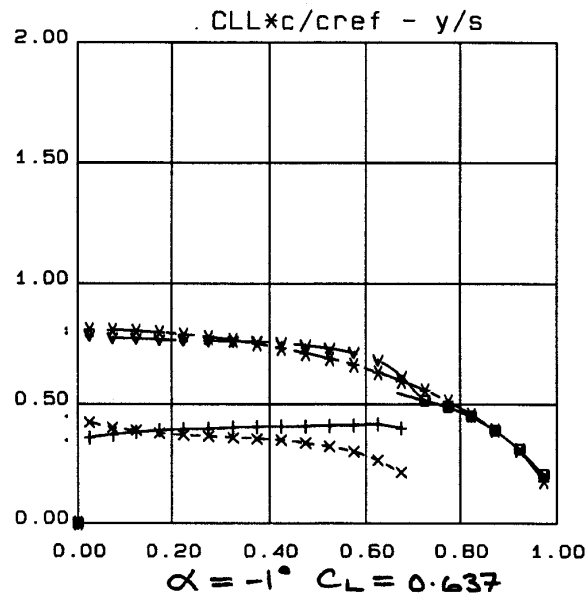


CL=1.25

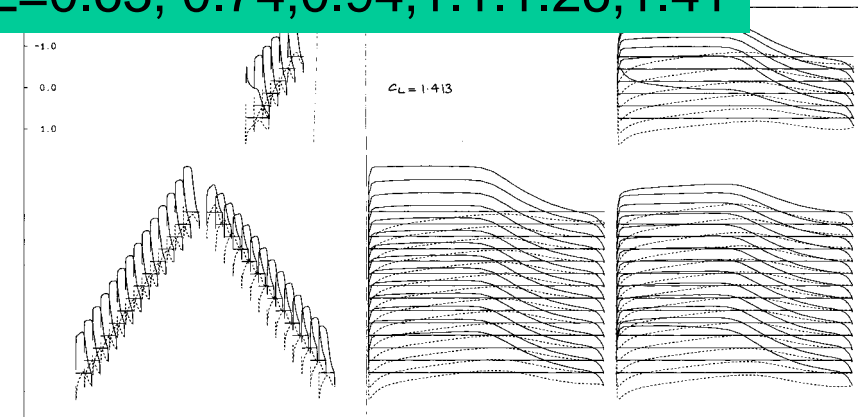
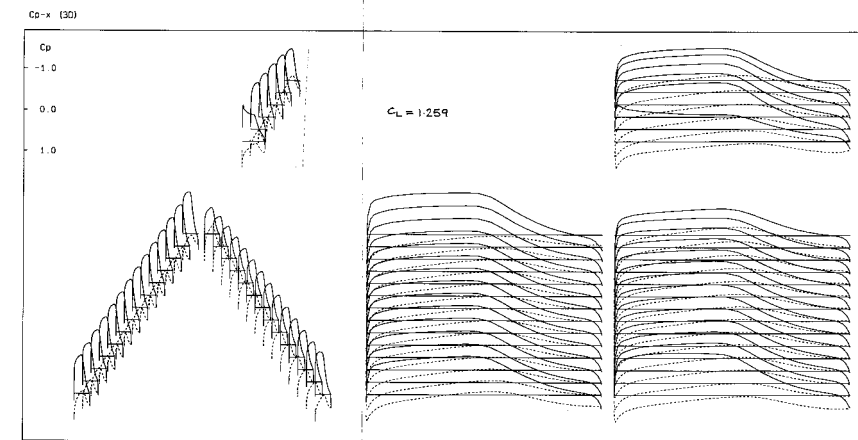
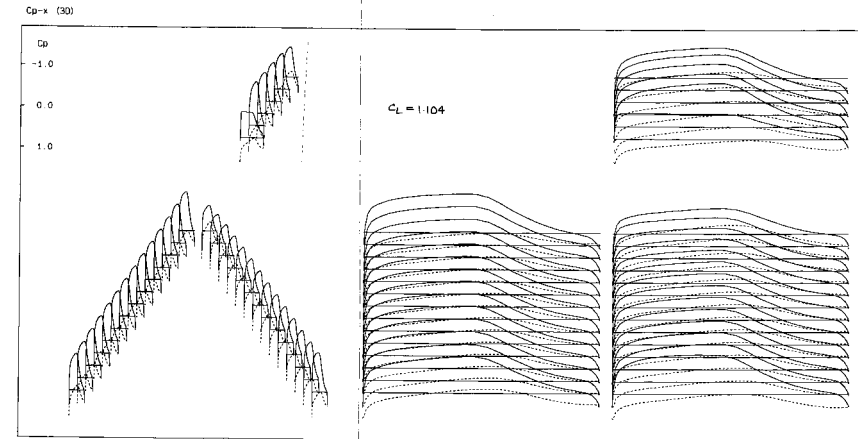
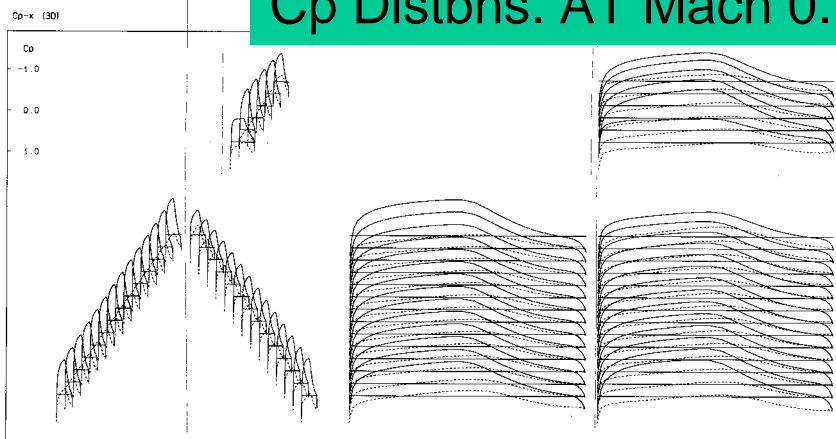
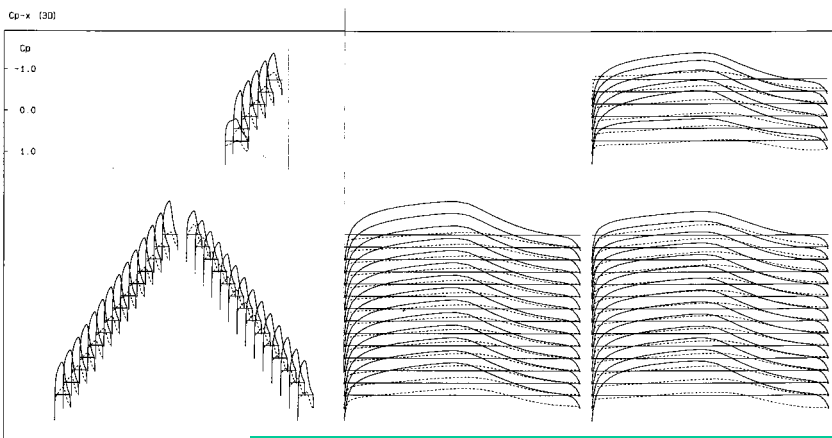
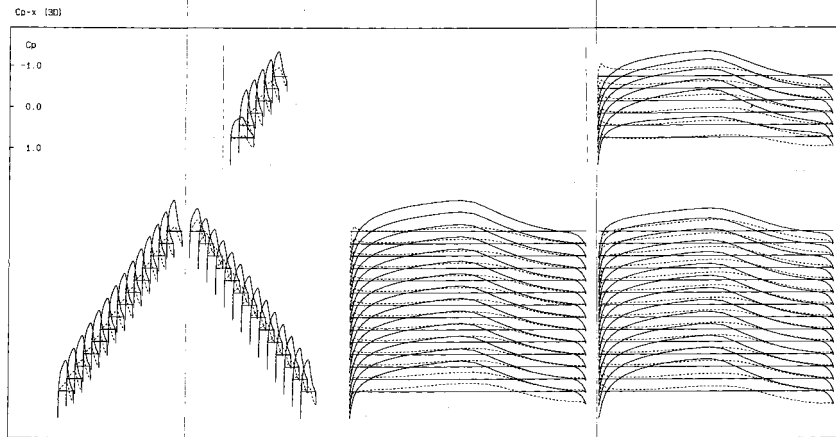
COMPARING UNCAMBERED & DESIGNED CONFIGS AT
SAME CL VALUES



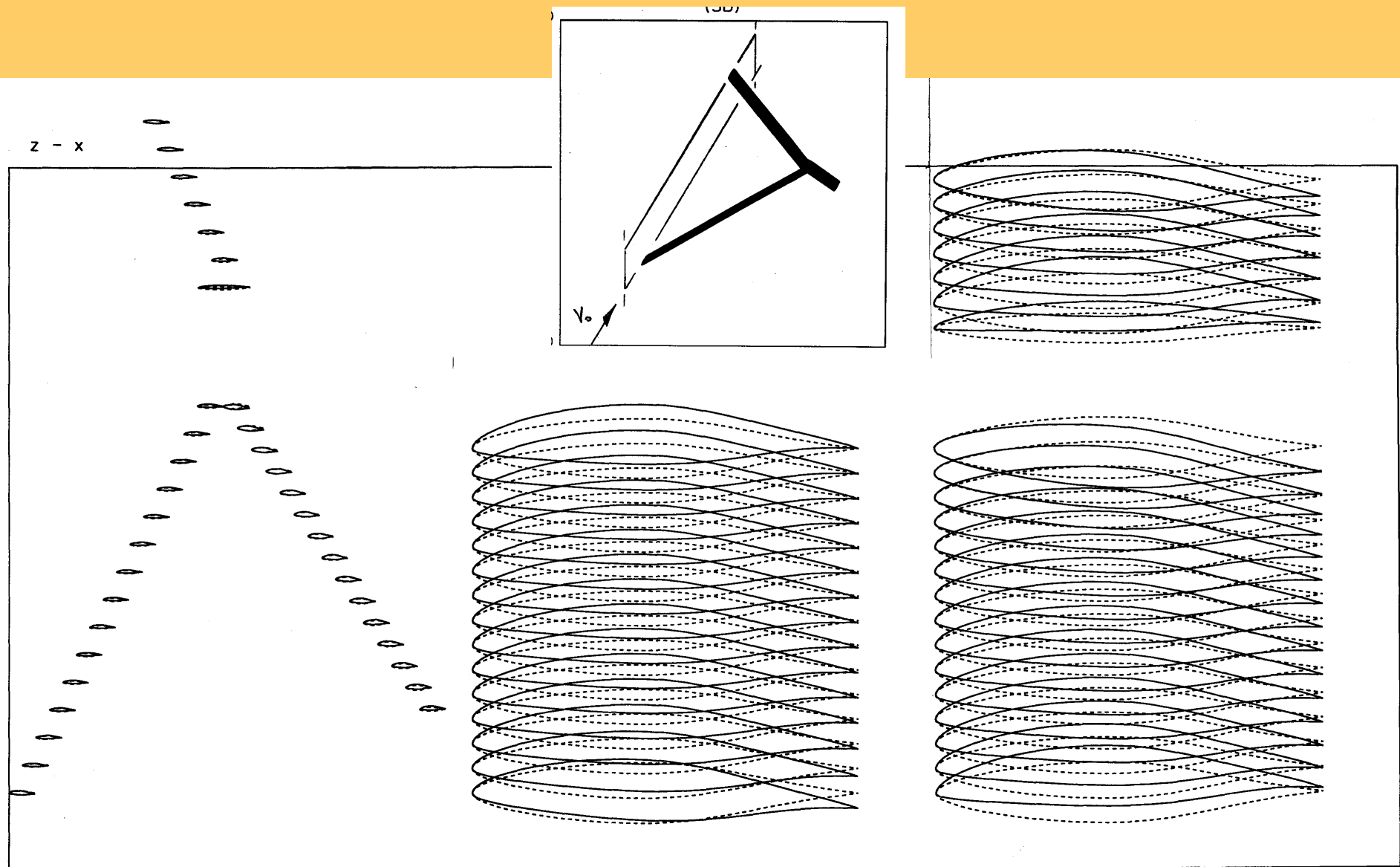
COMPARING UNCAMBERED & DESIGNED CONFIGS AT
SAME CL VALUES



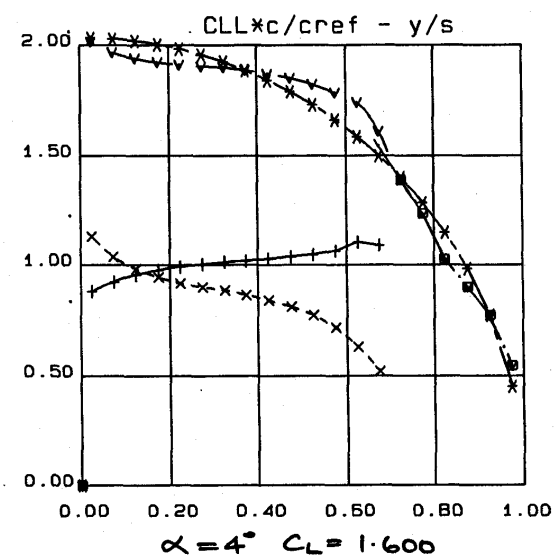
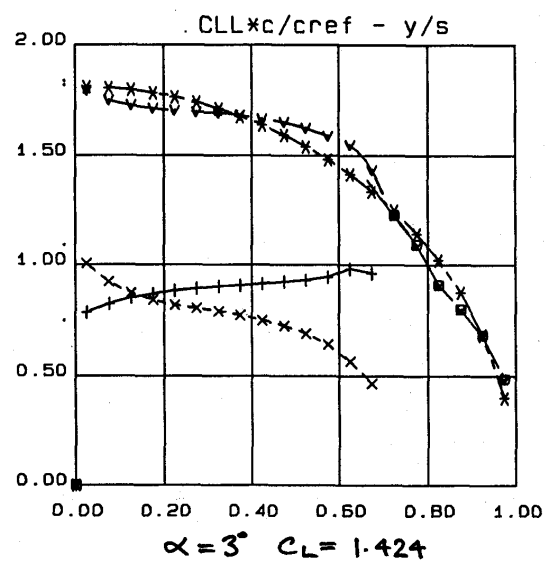
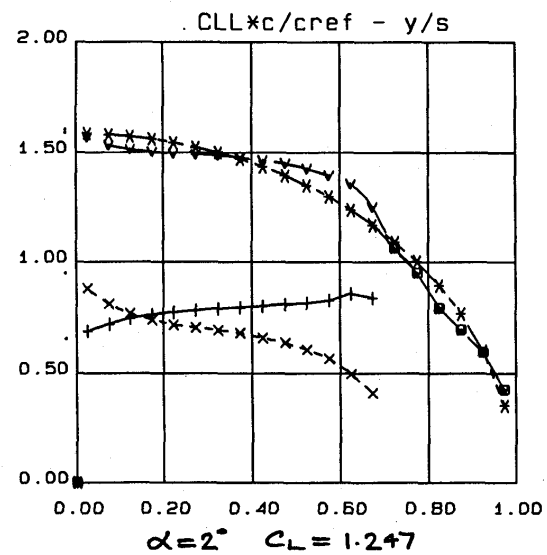
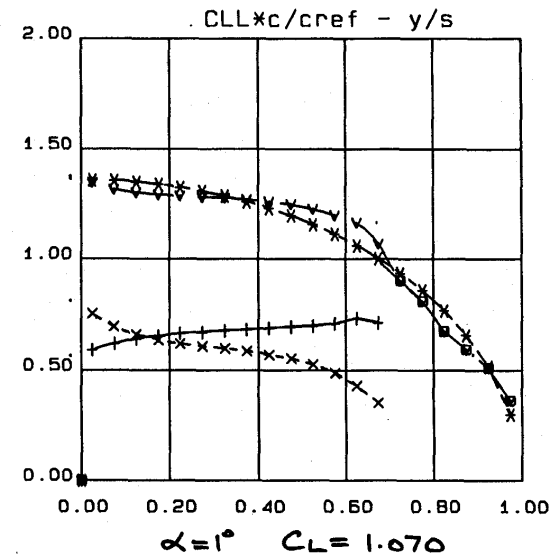
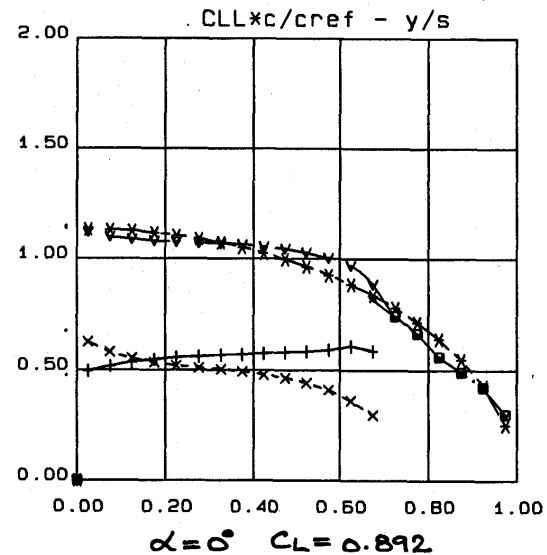
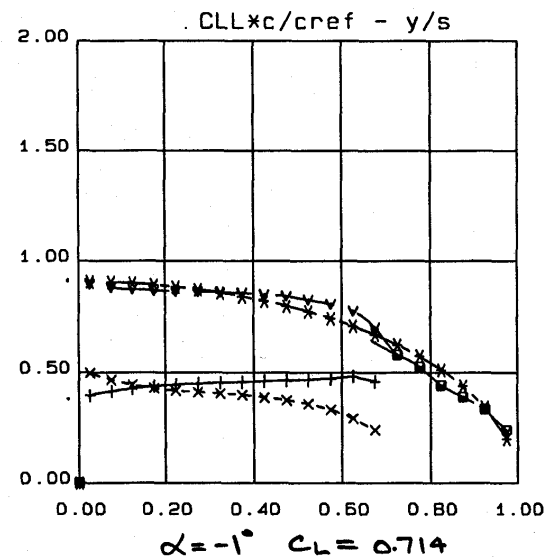
SPANWISE LOADINGS AT Mach 0.15, $C_L=0.63, 0.74, 0.94, 1.1, 1.26, 1.41$



Cp Distbns. AT Mach 0.15, $C_L=0.63, 0.74, 0.94, 1.1, 1.26, 1.41$

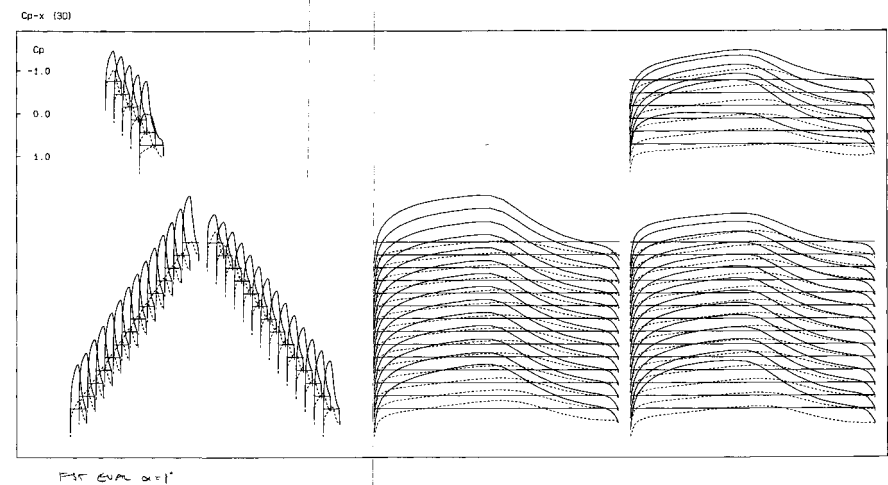
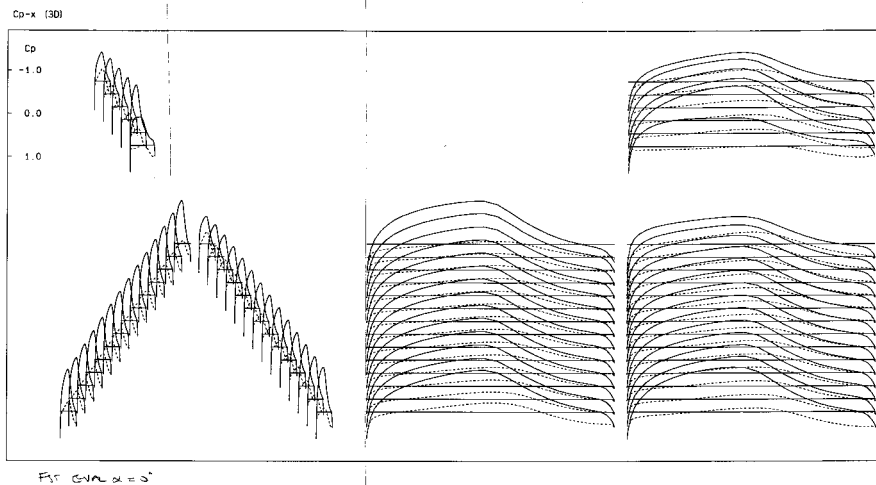
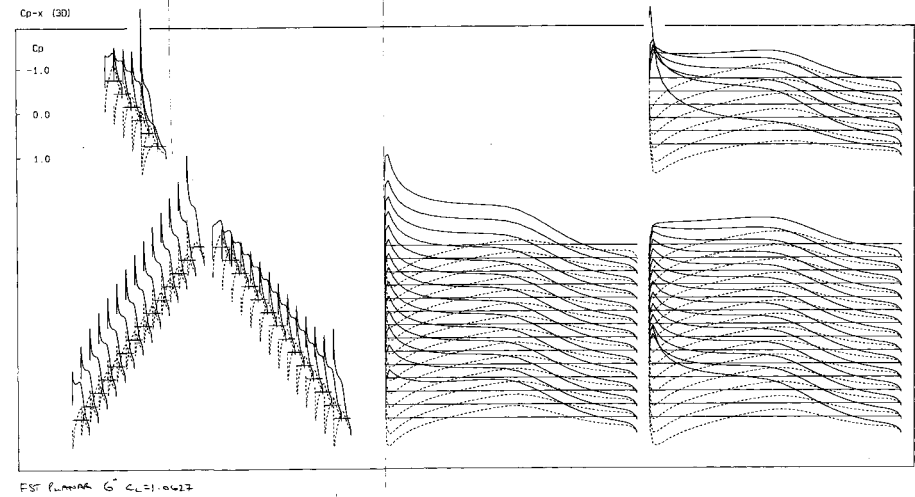
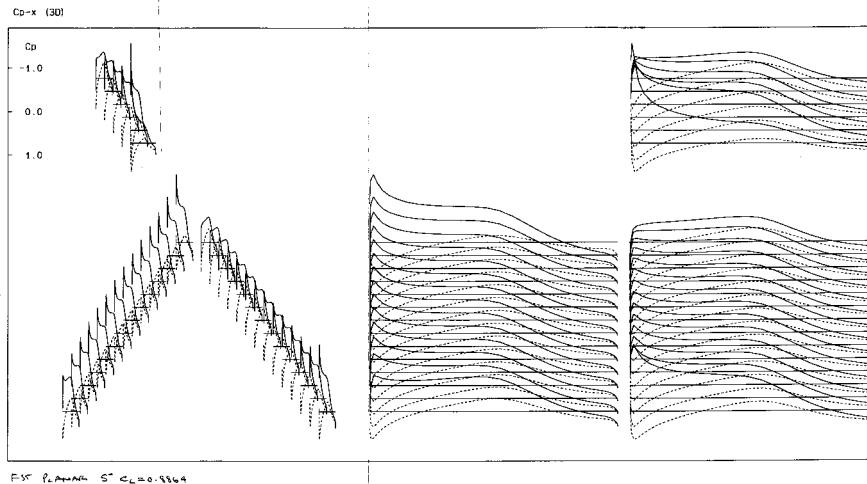


Forward Swept Tip FT1 Laminar



FST

SPANWISE LOADINGS AT Mach 0.6, $C_L = 0.72, 0.9, 1.07, 1.24, 1.43, 1.6$



CL=0.9

CL=1.07

COMPARING UNCAMBERED & DESIGNED CONFIGS AT
SAME CL VALUES

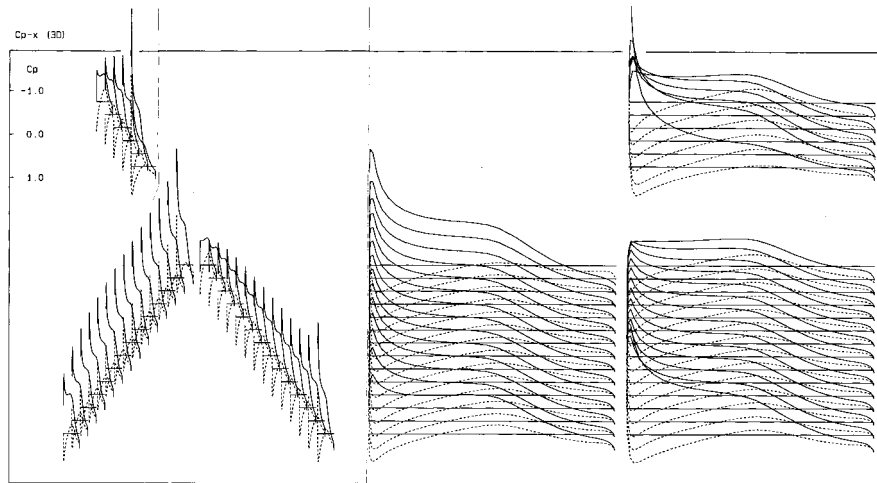


Fig 8. $\alpha = 7^\circ$ (uncambered)

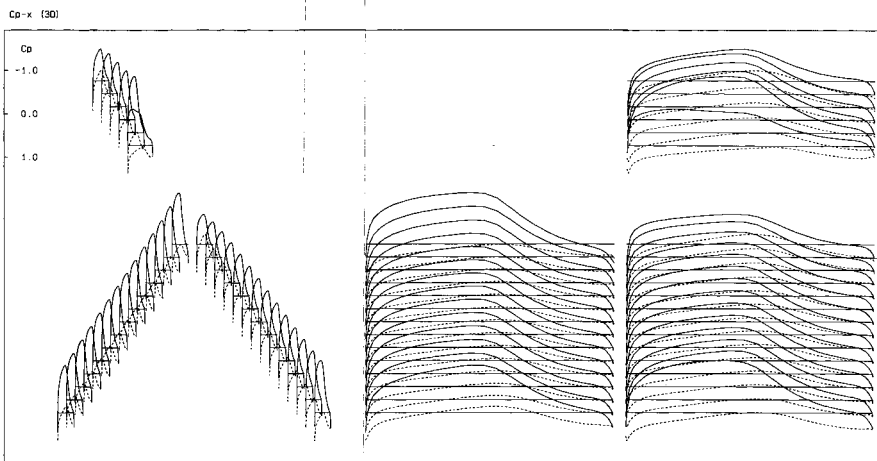


Fig 9. $\alpha = 2^\circ$ (uncambered)

CL=1.24

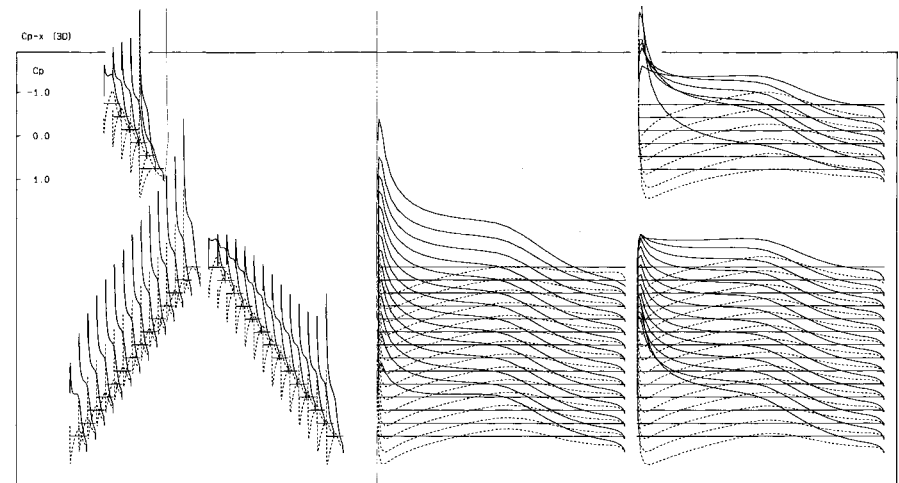


Fig 10. $\alpha = 7^\circ$ (designed)

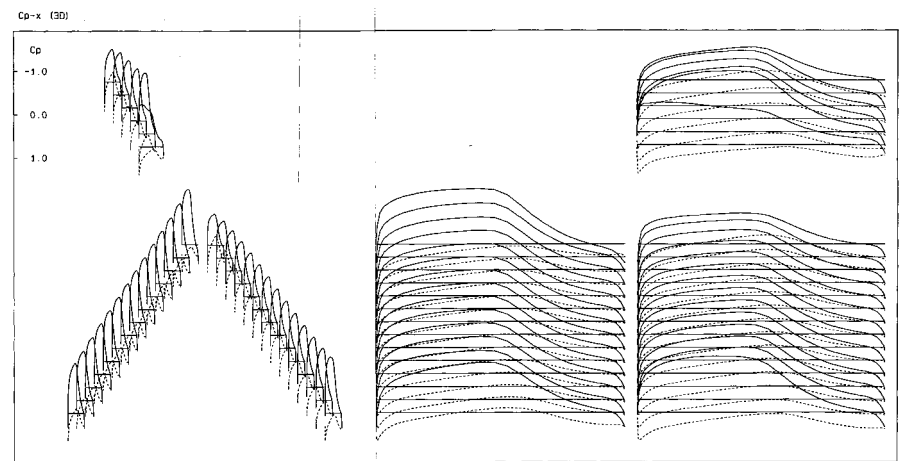
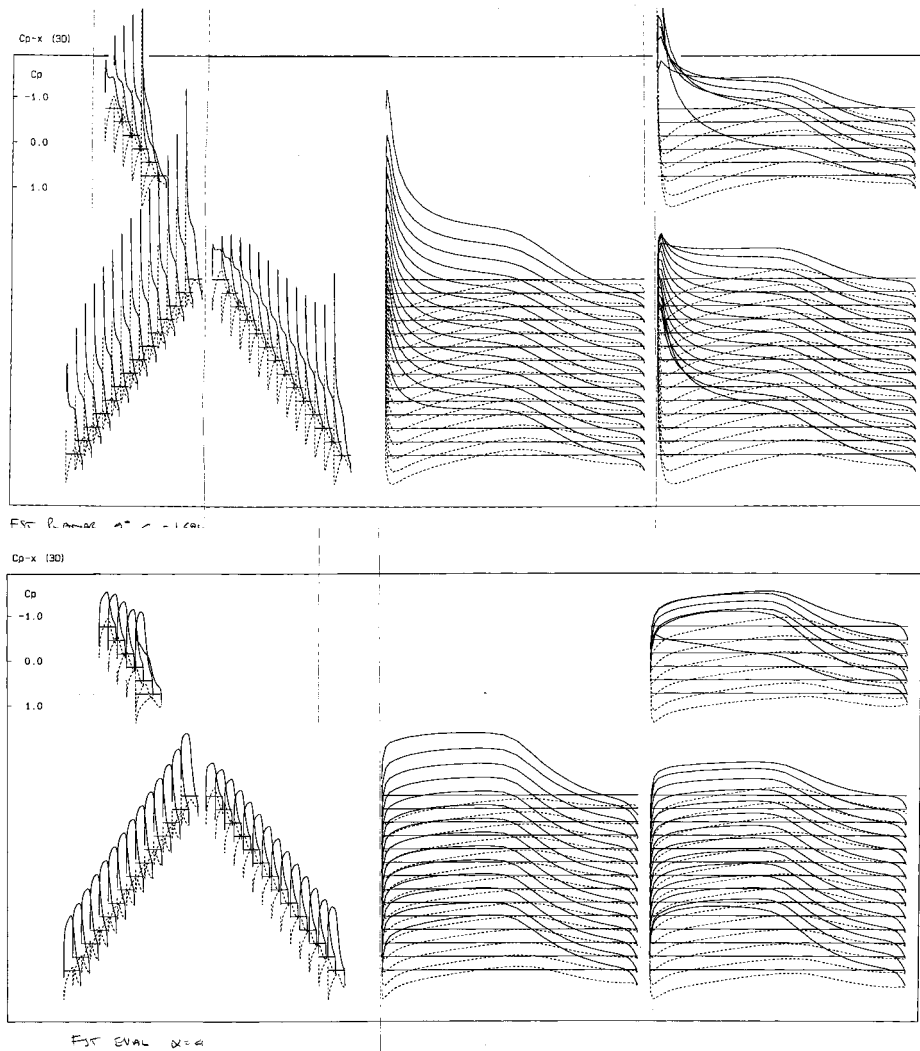


Fig 11. $\alpha = 2^\circ$ (designed)

CL=1.43

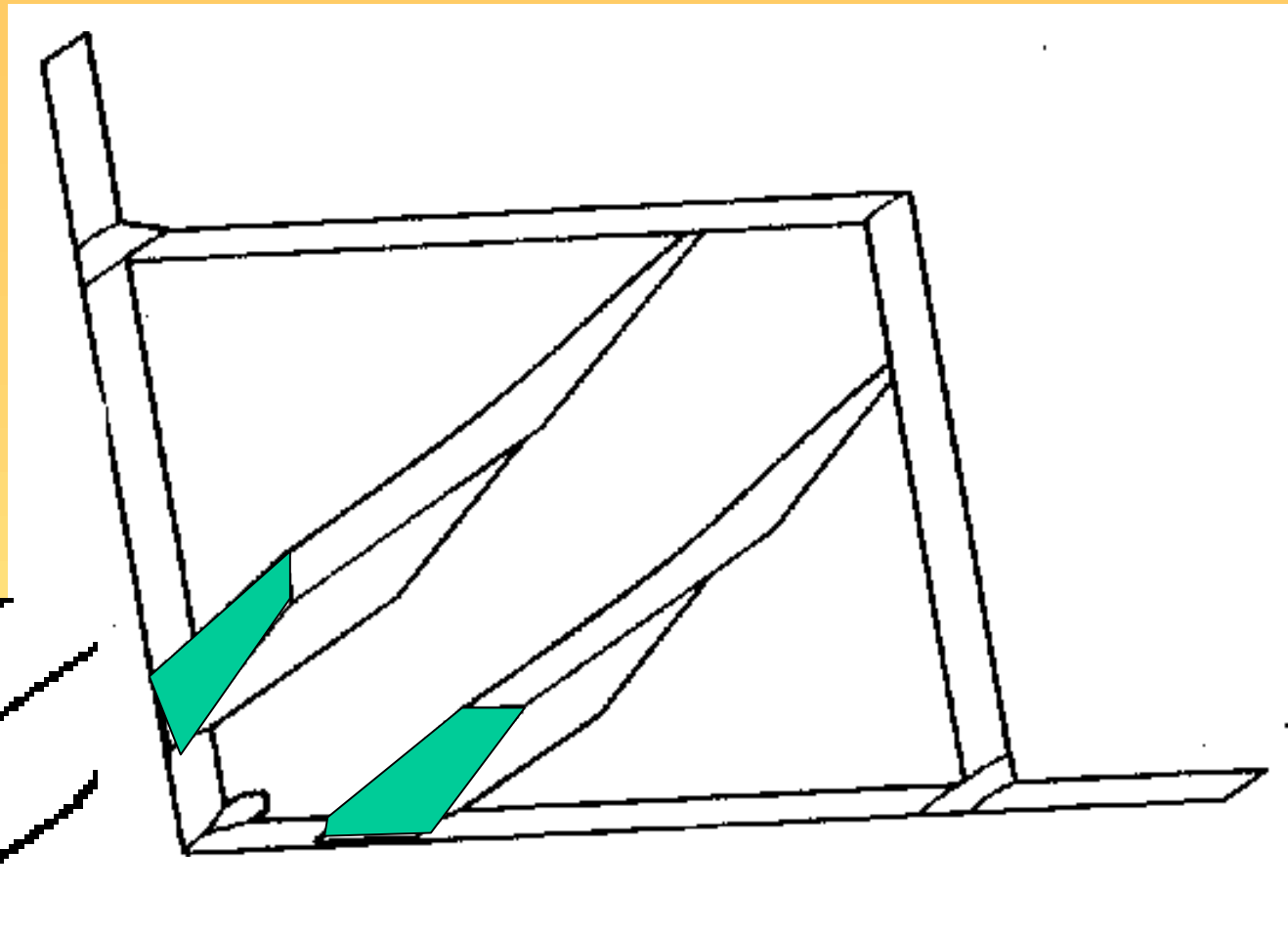
COMPARING UNCAMBERED & DESIGNED CONFIGS AT
SAME CL VALUES



Possibly Exceeding
Laminar limits at
Wing Junction

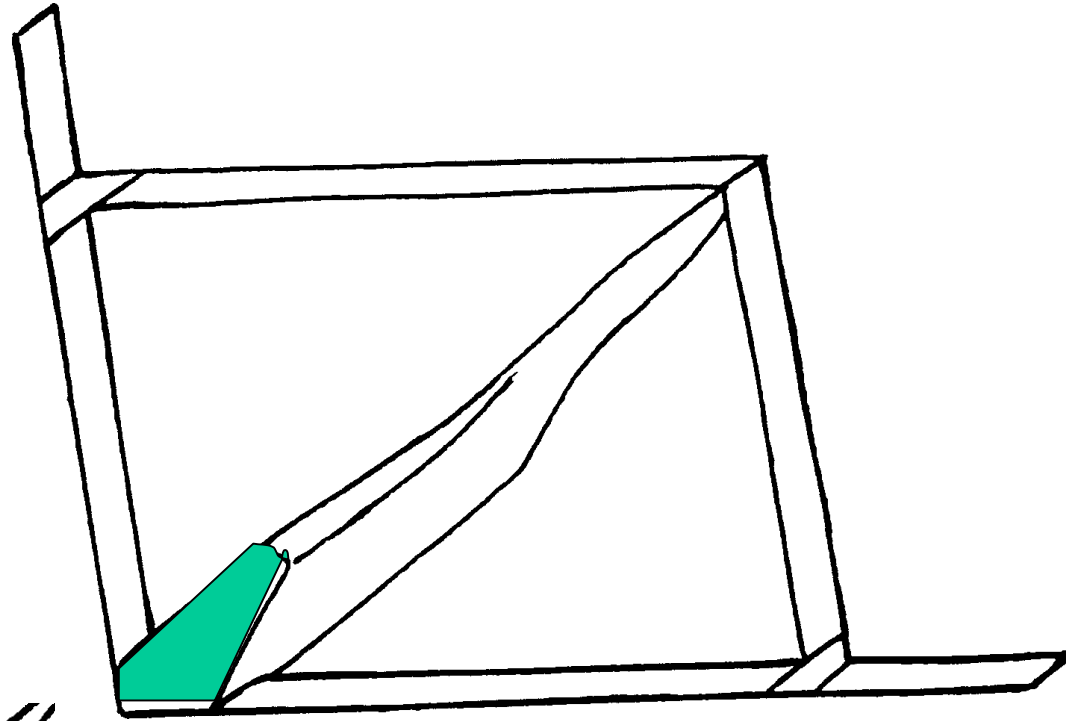
CL=1.6

COMPARING UNCAMBERED & DESIGNED CONFIGS AT
SAME CL VALUES

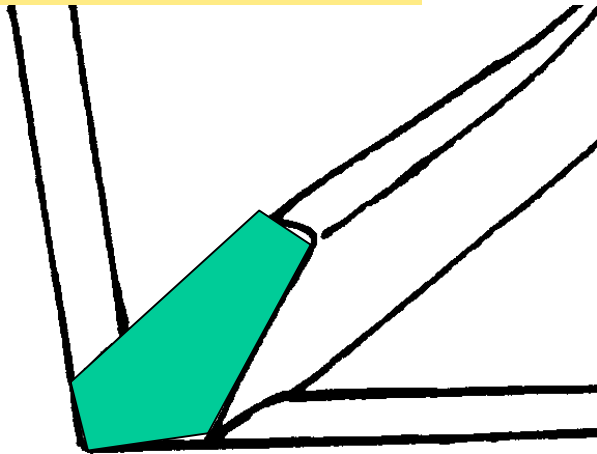


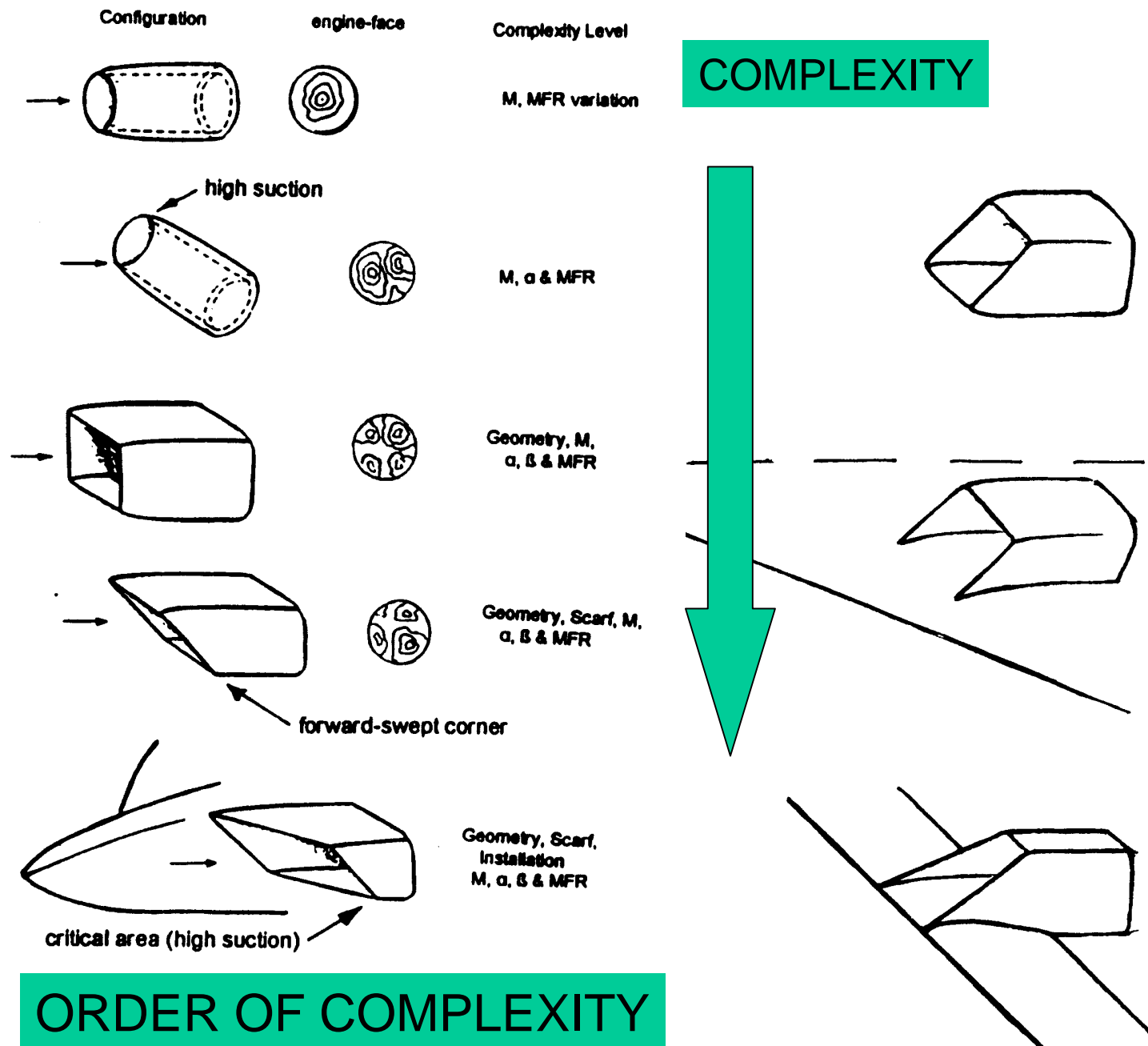
Twin Fuselage intakes

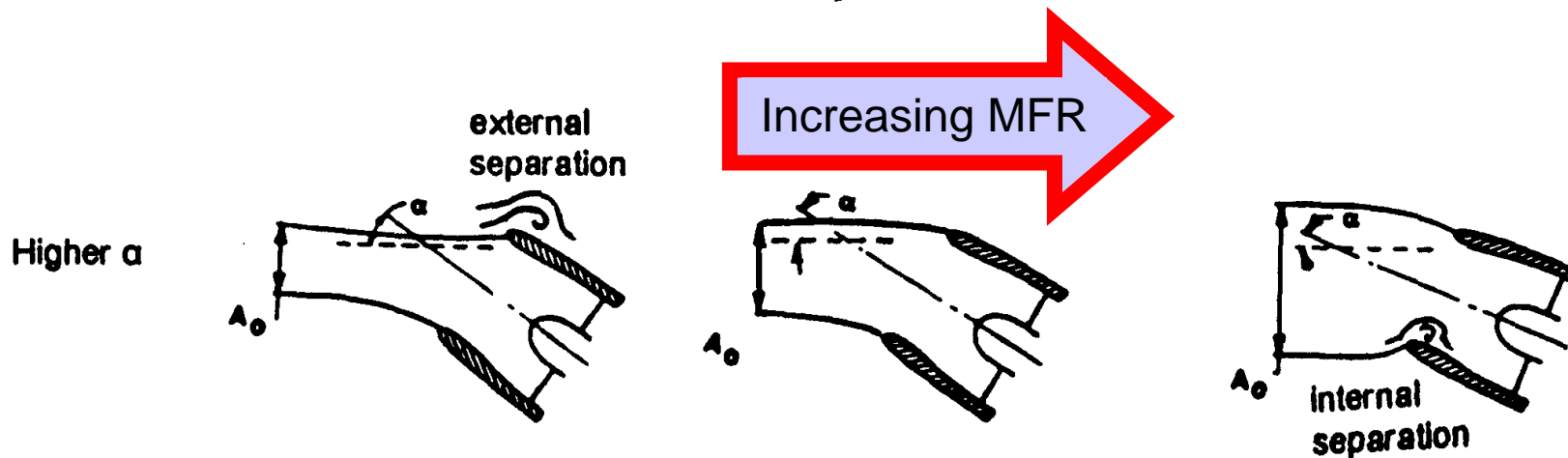
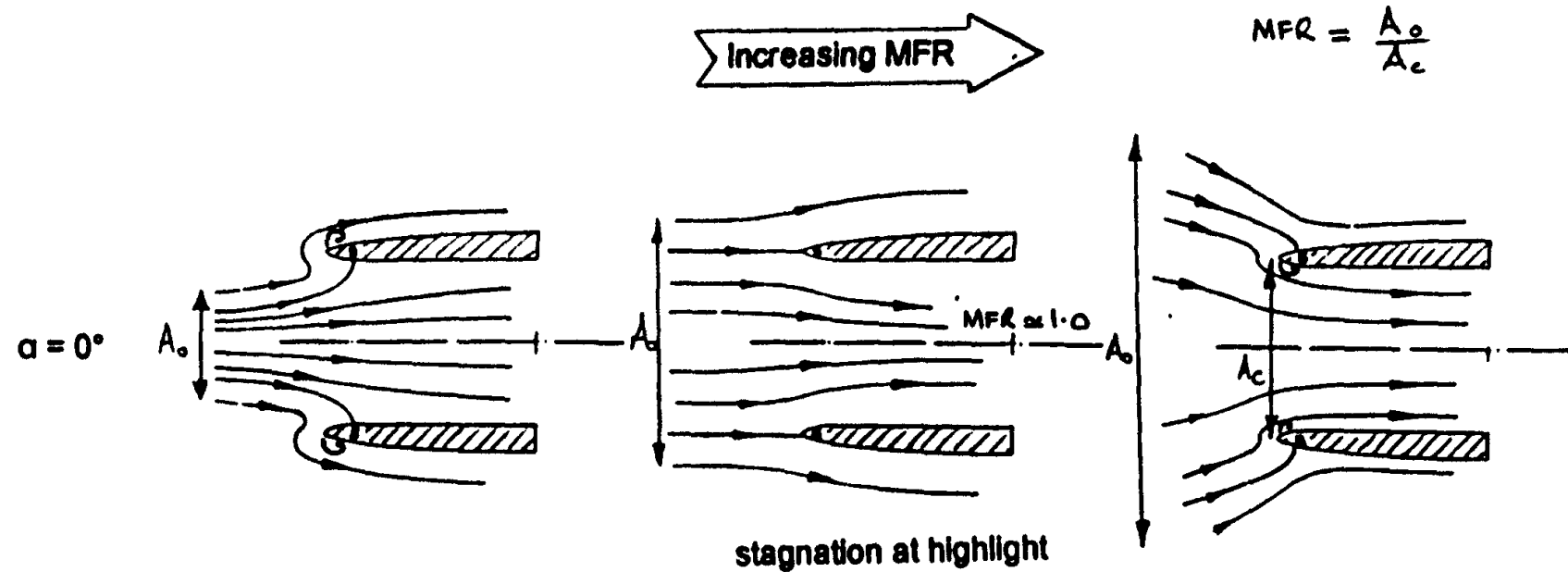
Propulsion Considerations



Central Fuselage intake

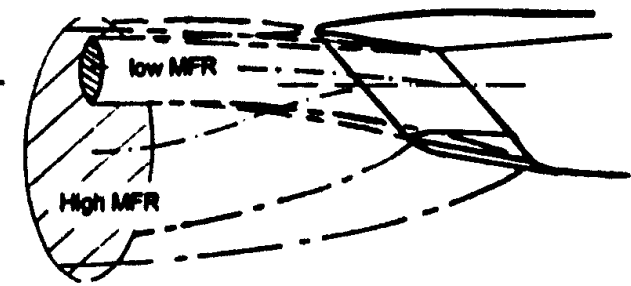
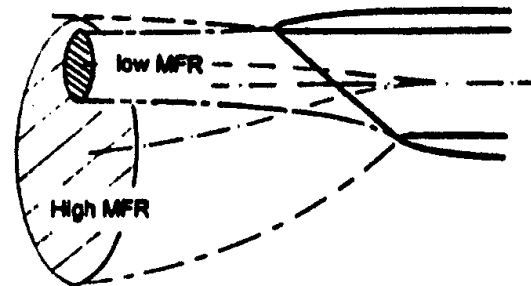
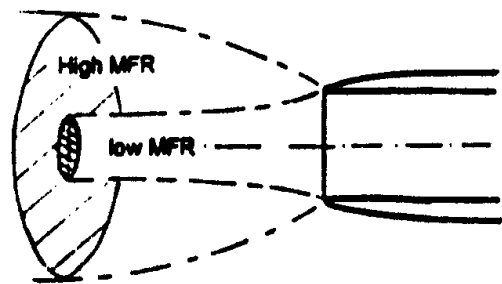




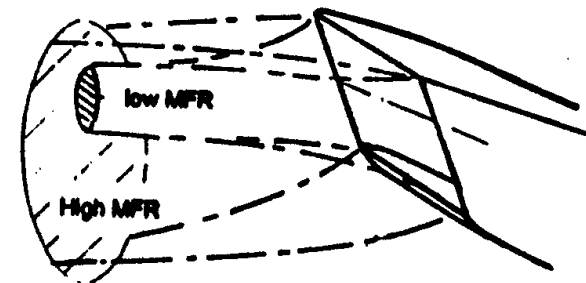
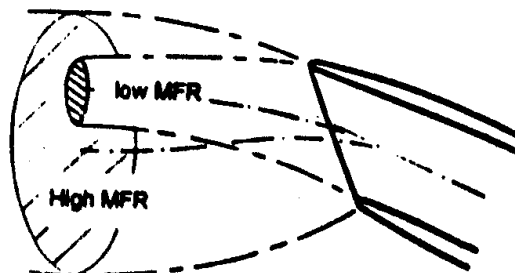
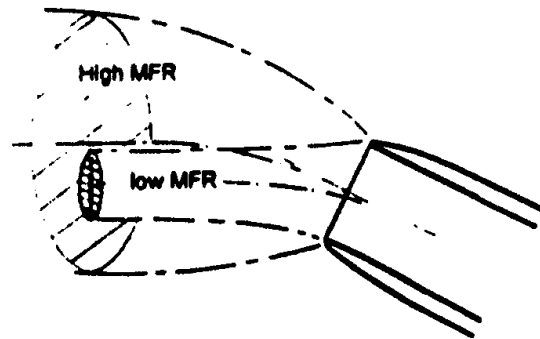


EFFECT OF MFR & α , ONSET OF EXTERNAL & INTERNAL LIP SEPARATION

UNSCARFED INTAKES



0 alpha



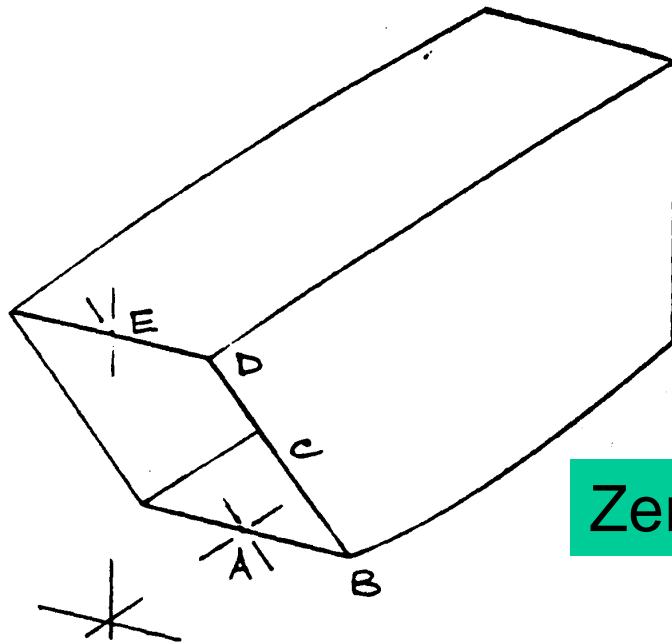
High alpha

Unscarfed

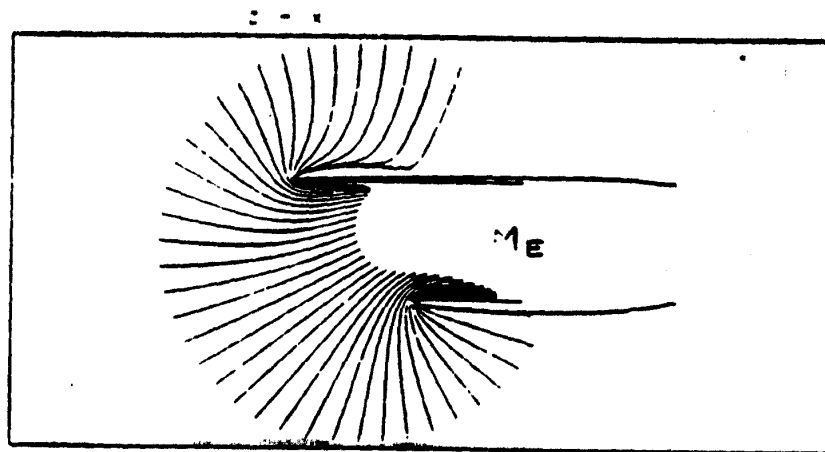
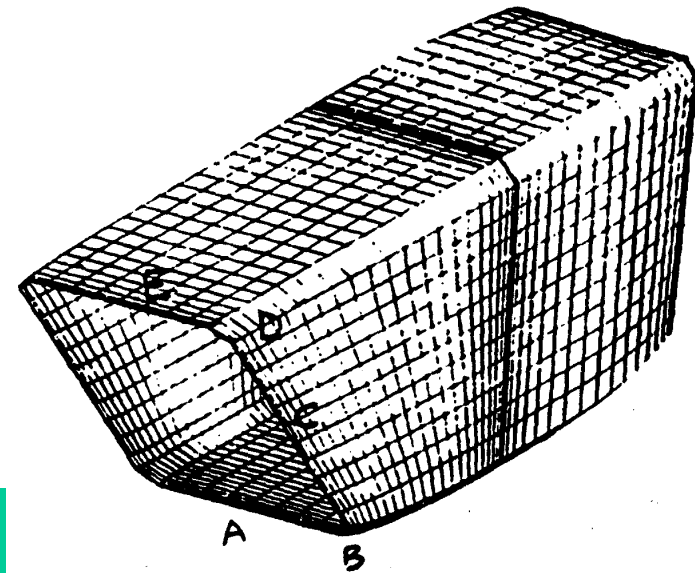
Scarfed

"Stealthy" Type

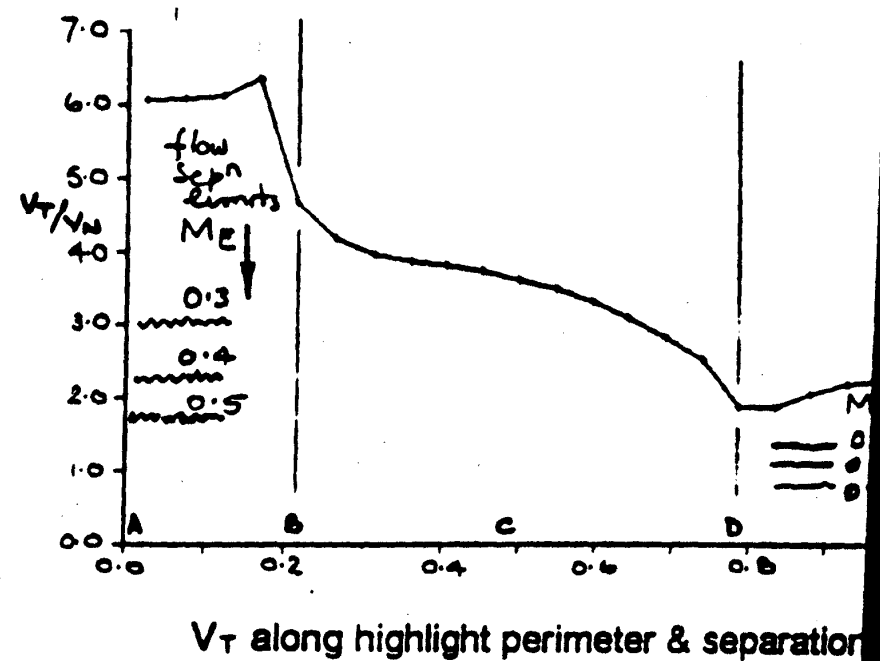
UNSCRAFED, SCARFED & 3-D STEALTHY INTAKES



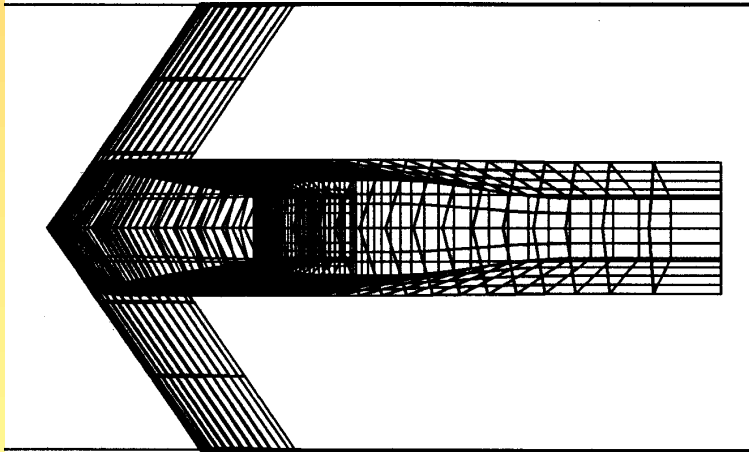
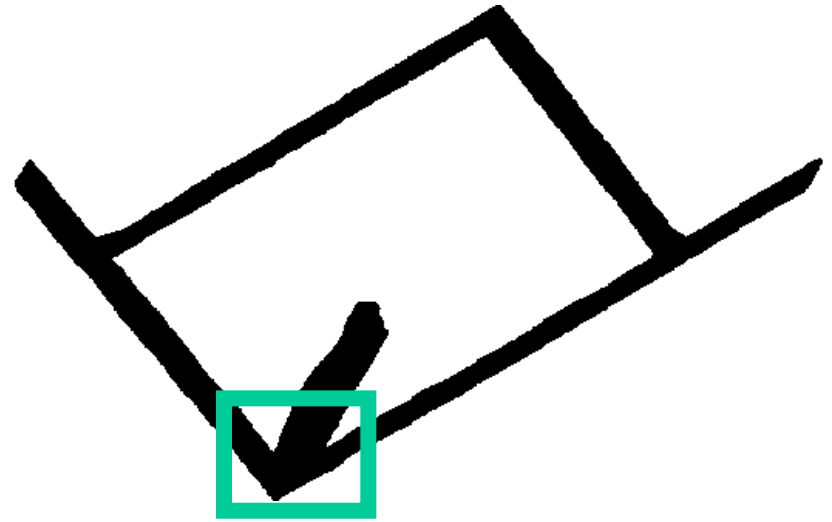
Zero speed



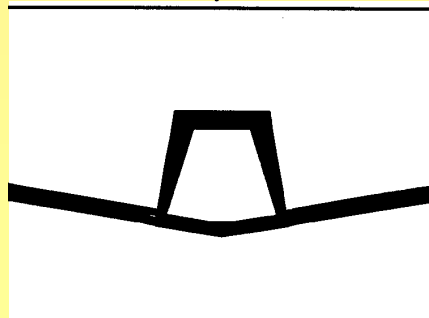
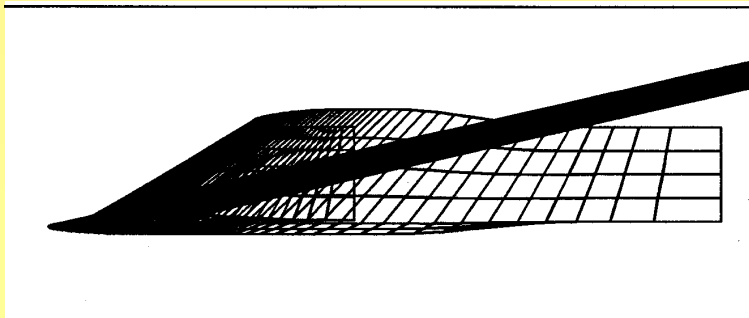
Streamlines, Symmetry plane



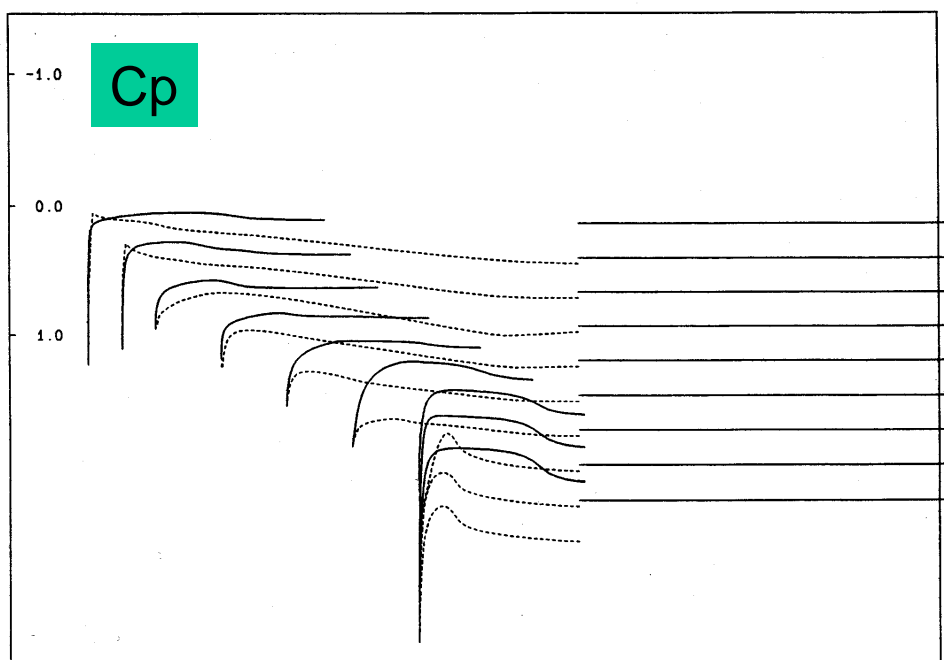
Central Intake Integration & Modelling



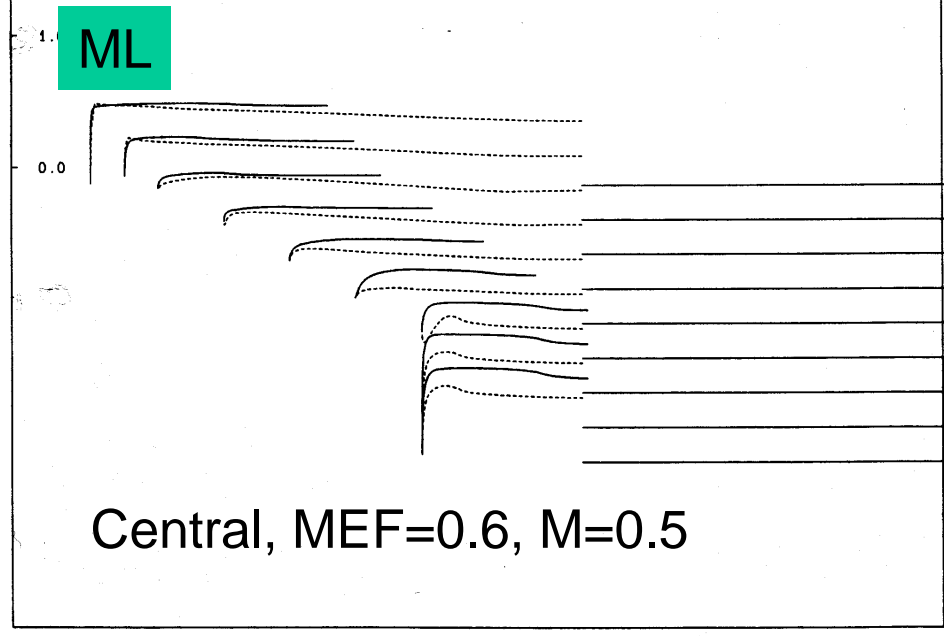
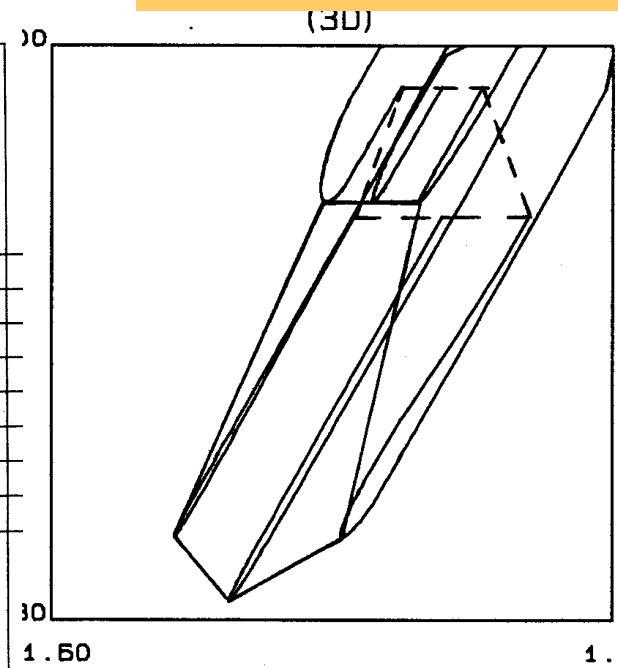
magnified



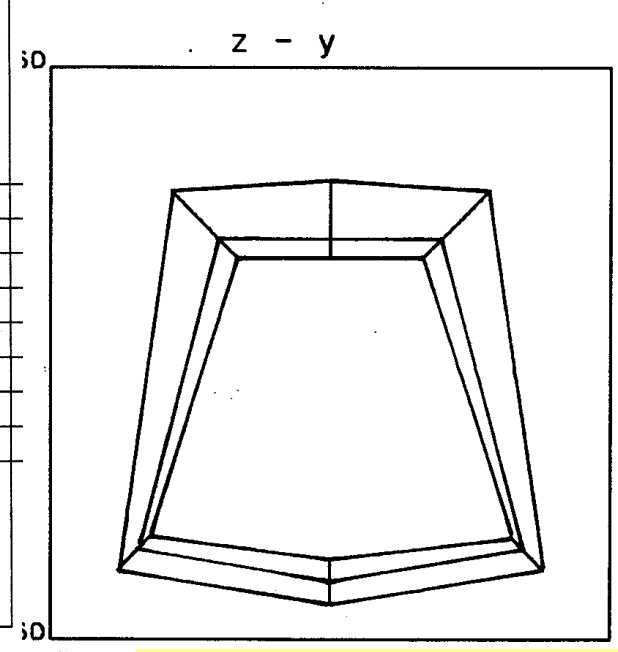
Cp-x (3D)



Cp

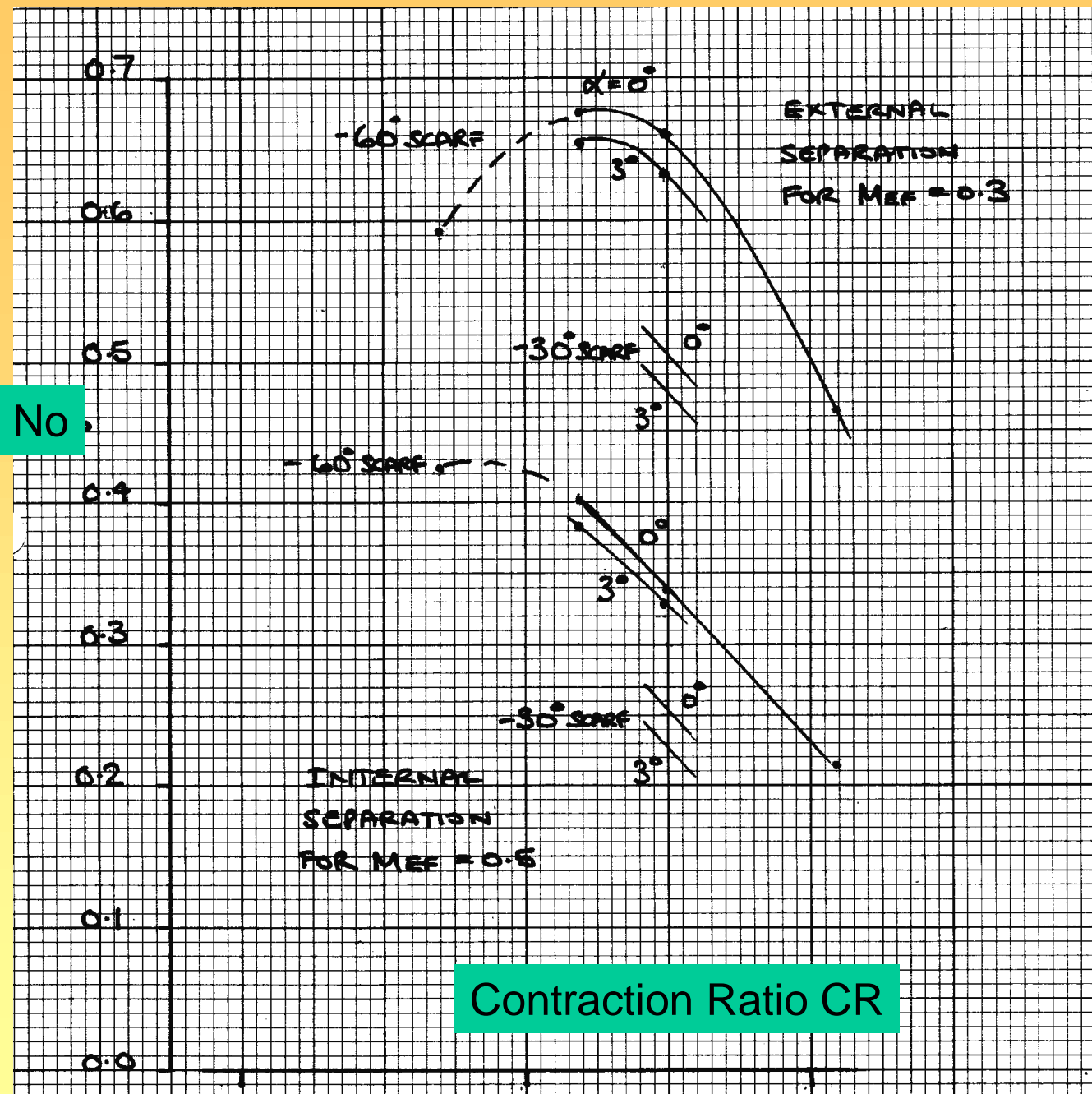


ML



Central, MEF=0.6, M=0.5

Mach No



Contraction Ratio CR

Intakes, Propulsion

- Shown a Preliminary set of Results
- Sizing is the first Concern
- Altitude of Operation !
- Off-Design
- Suitable Power-plants !
- Possibly Two needed
- Work Continues
- Experimental Work needed

Configuration & Structure

- Configuration / Layout
- What Light Materials
- One or two Fuselage
- Are such high AR craft feasible, structure
- Aero-elastic tailoring
- Manufacturing Constraints

Aerodynamics / Flow Control / Control

- Viscous Effects: Laminar Flow Extent
- Spanwise press. gradients
- Effect of Sweep, lower sweep Config. !
- Field performance
- Off-design, side-slip
- Controls location, pitch, directional & lateral
- Off-design
- Flow control, what & where!

Experimental work

- Difficulty in modelling large AR Configs
- Reynolds Number Considerations
- Laminar flow in WT !
- Half models
- Control effects not representative of full-scale
- A Radio Control Free-Flight Model !
- Propulsion Integration Considerations

Concluding Remarks

- Introduced HALE - UAV
- A Vision of Future – Sensor Craft Importance
- Joined-Wing Configs.
- 2-D Laminar Aerofoils
- Different Type of Swept-Tips in 3-D
- Aspects of 3-D Design
- LE Suction Control, Elliptic loadings, Neutral Stab.
- CFD Checks – Forward-Swept Root area
- Inverse Design Capabilities
- Intake Design – Preliminary Work
- Avenues for Further Work

***** Thank You for Listening *****

**So I hope, enough has been shown to
interest and inform you in the fast
moving field of Sensor-Craft
PLENTY of Further Work!**

Shall we try Comments and Questions?

